

In the name of God

Director of the course

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Isoparametric Formulation: Bar element

Rectangular Element

Isoparametric Formulation: Rectangular element

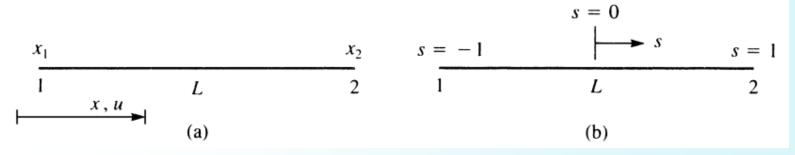
Numerical Integration

Higher-order shape functions

Bar element

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 Isoparametric element equations are formulated using a natural (or intrinsic) coordinate system s



• When the *s* and *x* axes are parallel to each other

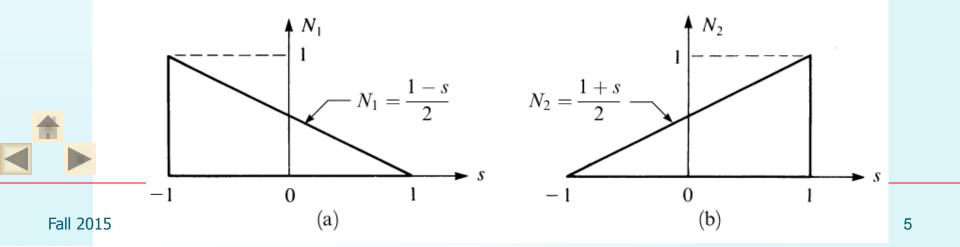
$$x = x_c + \frac{L}{2}s$$
 $s = [x - (x_1 + x_2)/2](2/(x_2 - x_1))$



- relating the natural coordinate to the global coordinate by: $x = a_1 + a_2 s$
- Solving for *a*₁ and *a*₂

$$x = \frac{1}{2} \left[(1-s)x_1 + (1+s)x_2 \right]$$

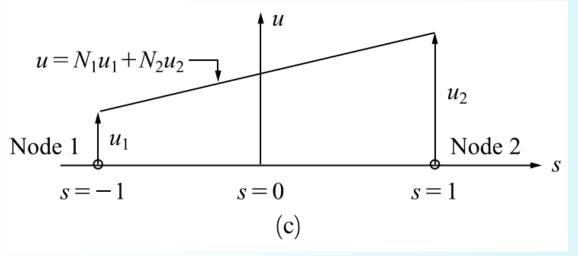
$$\{x\} = [N_1 \quad N_2] \begin{cases} x_1 \\ x_2 \end{cases}$$
 $N_1 = \frac{1-s}{2} \qquad N_2 = \frac{1+s}{2}$





• The displacement function within the bar is now defined by the same shape functions

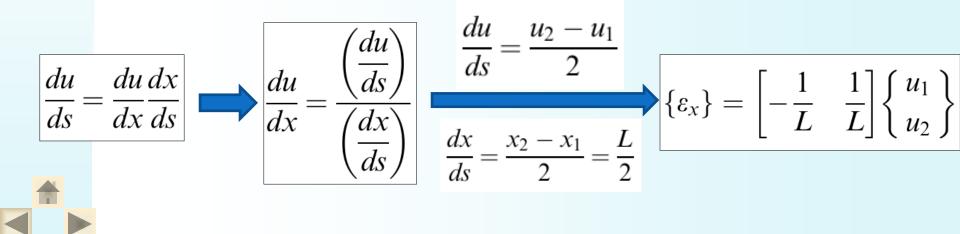
$$\{u\} = \begin{bmatrix} N_1 & N_2 \end{bmatrix} \left\{ \begin{array}{c} u_1 \\ u_2 \end{array} \right\}$$



• Since *u* and *x* are defined by the same shape functions at the same nodes, the element is called isoparametric .



- To construct the element stiffness matrix, we must determine the strain
- Therefore, we should determine the derivative of the displacement (*u*)with respect to *x*
- however, u is now a function of s



$$[B] = \begin{bmatrix} -\frac{1}{L} & \frac{1}{L} \end{bmatrix}$$

- [B] is ,in general, a function of *s*
- stiffness matrix

$$[k] = \int_0^L [B]^T [D] [B] A \, dx \qquad \int_0^L f(x) \, dx = \int_{-1}^1 f(s) |\underline{J}| \, ds$$

• |<u>J</u>| is called the Jacobian

$$|\underline{J}| = \frac{dx}{ds} = \frac{L}{2}$$

$$[k] = \frac{L}{2} \int_{-1}^{1} [B]^{T} E[B] A \, ds$$

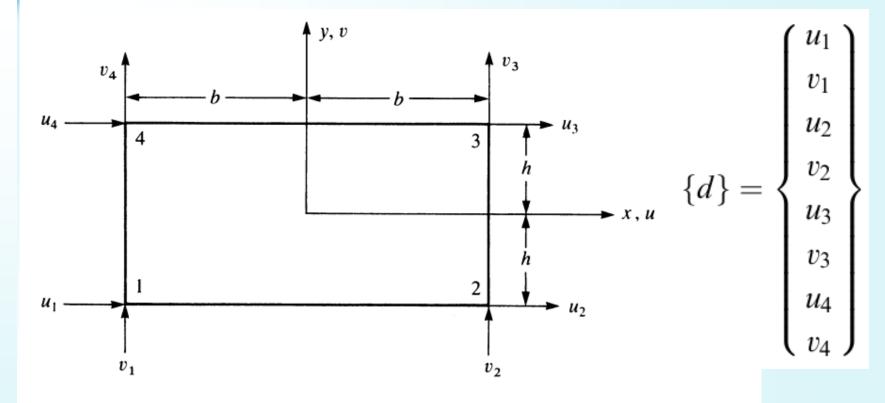
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$$\{\hat{f}_{b}\} = A \int_{0}^{L} [N]^{T} \{\hat{X}_{b}\} dx \quad (\hat{f}_{b}) = A \int_{-1}^{1} \left\{\frac{1-s}{2} \\ \frac{1+s}{2}\right\} \{\hat{X}_{b}\} \frac{L}{2} ds \quad (\hat{f}_{b}) = \frac{AL\hat{X}_{b}}{2} \left\{\frac{1}{1}\right\}$$

$$\{\hat{f}_{s}\} = \int_{0}^{L} [N_{s}]^{T} \{\hat{T}_{x}\} dx \quad (\hat{f}_{s}) = \int_{-1}^{1} \left\{\frac{1-s}{2} \\ \frac{1+s}{2}\right\} \{\hat{T}_{x}\} \frac{L}{2} ds \quad (\hat{f}_{s}) = \hat{T}_{x} \frac{L}{2} \left\{\frac{1}{1}\right\}$$

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Basic four-node rectangular element with nodal degrees of freedom

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$$u(x, y) = a_1 + a_2 x + a_3 y + a_4 x y$$
$$v(x, y) = a_5 + a_6 x + a_7 y + a_8 x y$$

$$u(x, y) = \frac{1}{4bh} [(b - x)(h - y)u_1 + (b + x)(h - y)u_2 + (b + x)(h + y)u_3 + (b - x)(h + y)u_4]$$
$$v(x, y) = \frac{1}{4bh} [(b - x)(h - y)v_1 + (b + x)(h - y)v_2 + (b + x)(h + y)v_3 + (b - x)(h + y)v_4]$$

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$$\{\psi\} = [N]\{d\}$$

$$N_{1} = \frac{(b-x)(h-y)}{4bh} \qquad N_{2} = \frac{(b+x)(h-y)}{4bh}$$

$$N_{3} = \frac{(b+x)(h+y)}{4bh} \qquad N_{4} = \frac{(b-x)(h+y)}{4bh}$$

$$\left\{ \begin{array}{c} u\\ v\\ v \end{array} \right\} = \begin{bmatrix} N_{1} & 0 & N_{2} & 0 & N_{3} & 0 & N_{4} & 0\\ 0 & N_{1} & 0 & N_{2} & 0 & N_{3} & 0 & N_{4} \end{bmatrix} \begin{bmatrix} u_{1}\\ v_{1}\\ u_{2}\\ v_{2}\\ u_{3}\\ v_{3}\\ u_{4}\\ v_{4} \end{bmatrix}$$

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$$\begin{cases} \varepsilon_x \\ \varepsilon_y \\ \gamma_{xy} \end{cases} = \begin{cases} \frac{\partial u}{\partial x} \\ \frac{\partial v}{\partial y} \\ \frac{\partial u}{\partial y} + \frac{\partial v}{\partial x} \end{cases}$$
$$[B] = \frac{1}{4bh} \begin{bmatrix} -(h-y) & 0 & (h-y) & 0 \\ 0 & -(b-x) & 0 & -(b+x) \\ -(b-x) & -(h-y) & -(b+x) & (h-y) \\ -(b-x) & -(h-y) & -(b+x) & (h-y) \\ \end{cases}$$
$$\begin{pmatrix} (h+y) & 0 & -(h+y) & 0 \\ 0 & (b+x) & (h-y) & 0 \\ 0 & (b+x) & 0 & (b-x) \\ (b+x) & (h+y) & (b-x) & -(h+y) \end{bmatrix}$$

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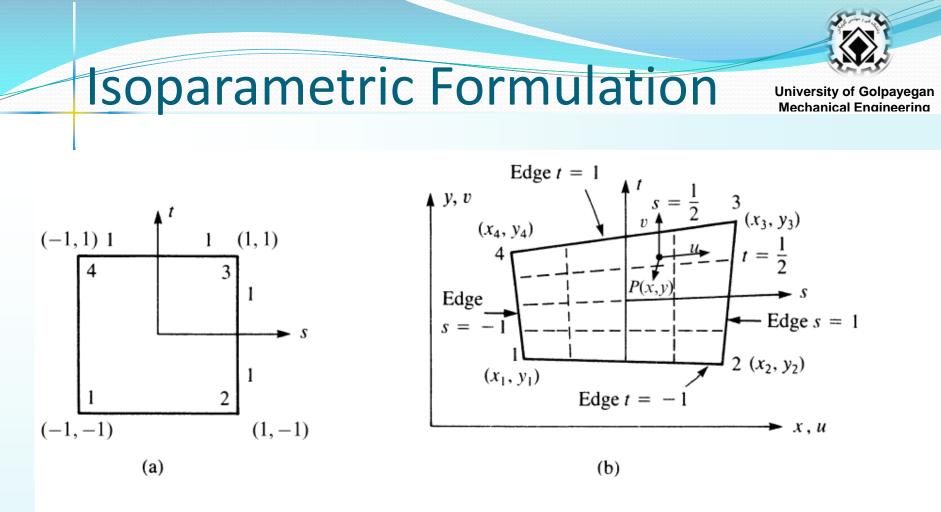
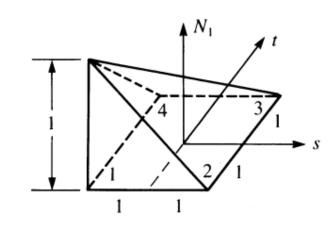
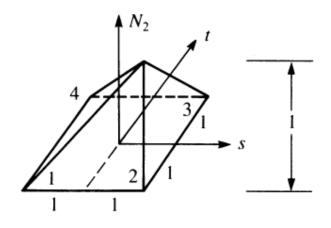


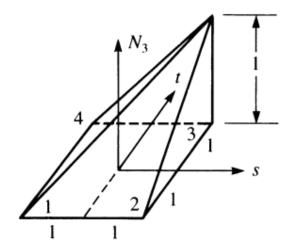
Figure 10–4 (a) Linear square element in *s*-*t* coordinates and (b) square element mapped into quadrilateral in *x*-*y* coordinates whose size and shape are determined by the eight nodal coordinates x_1, y_1, \ldots, y_4

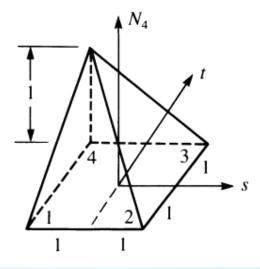








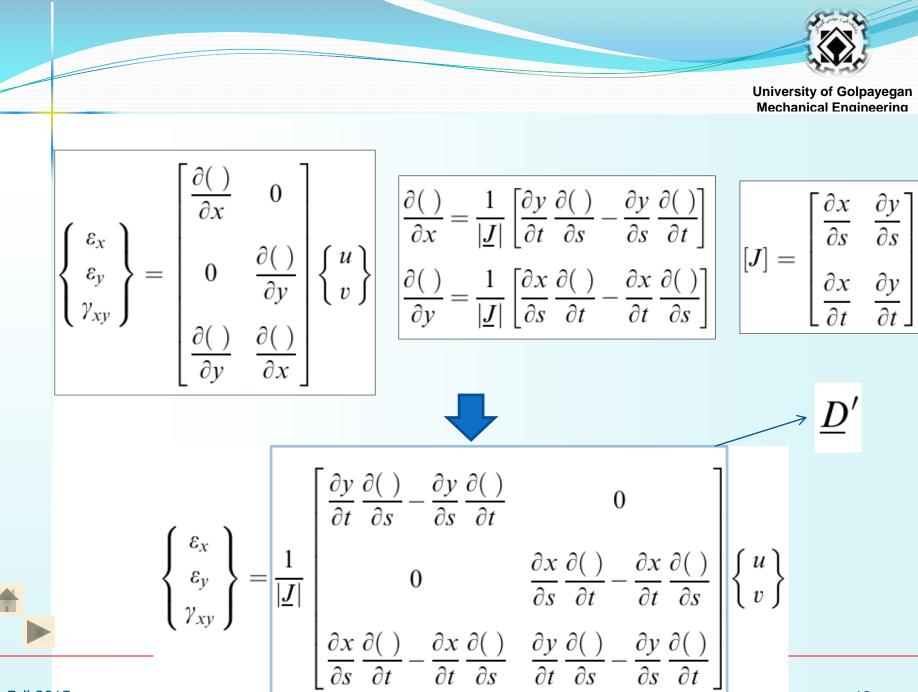




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17



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18

$$\underline{\varepsilon} = \underline{D}' \underline{N} \underline{d}$$

$$\underline{\underline{B}} = \underline{\underline{D}}' \quad \underline{\underline{N}} \\ (3 \times 8) \quad (3 \times 2) \quad (2 \times 8)$$

$$\underline{B}(s,t) = \frac{1}{|\underline{J}|} \begin{bmatrix} \underline{B}_1 & \underline{B}_2 & \underline{B}_3 & \underline{B}_4 \end{bmatrix}$$

$$\underline{B}_{i} = \begin{bmatrix} a(N_{i,s}) - b(N_{i,t}) & 0\\ 0 & c(N_{i,t}) - d(N_{i,s})\\ c(N_{i,t}) - d(N_{i,s}) & a(N_{i,s}) - b(N_{i,t}) \end{bmatrix}$$

$$a = \frac{1}{4} [y_1(s-1) + y_2(-1-s) + y_3(1+s) + y_4(1-s)]$$

$$b = \frac{1}{4} [y_1(t-1) + y_2(1-t) + y_3(1+t) + y_4(-1-t)]$$

$$c = \frac{1}{4} [x_1(t-1) + x_2(1-t) + x_3(1+t) + x_4(-1-t)]$$

$$d = \frac{1}{4} [x_1(s-1) + x_2(-1-s) + x_3(1+s) + x_4(1-s)]$$

Jacobian

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$$\begin{split} \begin{bmatrix} J \end{bmatrix} &= \begin{bmatrix} \frac{\partial x}{\partial s} & \frac{\partial y}{\partial s} \\ \frac{\partial x}{\partial t} & \frac{\partial y}{\partial t} \end{bmatrix} & x = \frac{1}{4} \begin{bmatrix} (1-s)(1-t)x_1 + (1+s)(1-t)x_2 \\ + (1+s)(1+t)x_3 + (1-s)(1+t)x_4 \end{bmatrix} \\ y = \frac{1}{4} \begin{bmatrix} (1-s)(1-t)y_1 + (1+s)(1-t)y_2 \\ + (1+s)(1+t)y_3 + (1-s)(1+t)y_4 \end{bmatrix} \\ &+ (1+s)(1+t)y_3 + (1-s)(1+t)y_4 \end{bmatrix} \\ \begin{bmatrix} J \end{bmatrix} &= \frac{1}{8} \{ X_c \}^T \begin{bmatrix} 0 & 1-t & t-s & s-1 \\ t-1 & 0 & s+1 & -s-t \\ s-t & -s-1 & 0 & t+1 \\ 1-s & s+t & -t-1 & 0 \\ & \{ X_c \}^T = \begin{bmatrix} x_1 & x_2 & x_3 & x_4 \end{bmatrix} \\ & \{ Y_c \} = \begin{cases} y_1 \\ y_2 \\ y_3 \\ y_4 \end{cases} \end{split}$$

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20



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- *B* is a function of *s* and *t* in both the numerator and the denominator

• Therefore the integration to determine the element stiffness matrix is usually done numerically.

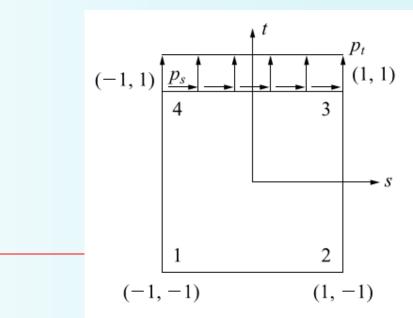
Body forces

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The element body-force matrix will now be determined from

$$\begin{cases} \{f_b\} \\ (8 \times 1) \end{cases} = \int_{-1}^{1} \int_{-1}^{1} [N]^T \{X\} h |\underline{J}| \, ds \, dt \qquad (10.3.28)$$

Like the stiffness matrix, the body-force matrix in Eq. (10.3.28) has to be evaluated by numerical integration.



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Surface forces

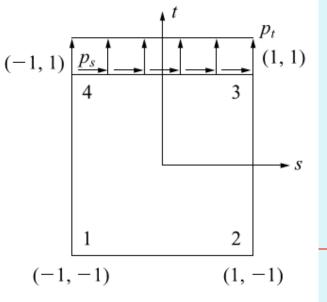
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$$\begin{cases} \{f_s\} \\ (4 \times 1) \end{cases} = \int_{-1}^{1} \begin{bmatrix} N_s \end{bmatrix}^T \{T\} h \frac{L}{2} ds$$

$$\begin{cases} f_{s3s} \\ f_{s3t} \\ f_{s4s} \\ f_{s4t} \end{cases} = \int_{-1}^{1} \begin{bmatrix} N_3 & 0 & N_4 & 0 \\ 0 & N_3 & 0 & N_4 \end{bmatrix}^T \begin{vmatrix} p_s \\ p_t \end{vmatrix} h \frac{L}{2} ds$$
evaluated along $t = 1$

- N₁=0 and N₂=0 along edge t=1
- Therefore, no nodal forces exist at nodes 1 and 2

$$\{f_s\} = h \frac{L}{2} \begin{bmatrix} 0 & 0 & 0 & p_s & p_t & p_s & p_t \end{bmatrix}^T$$





Example 10.1 : p. 461

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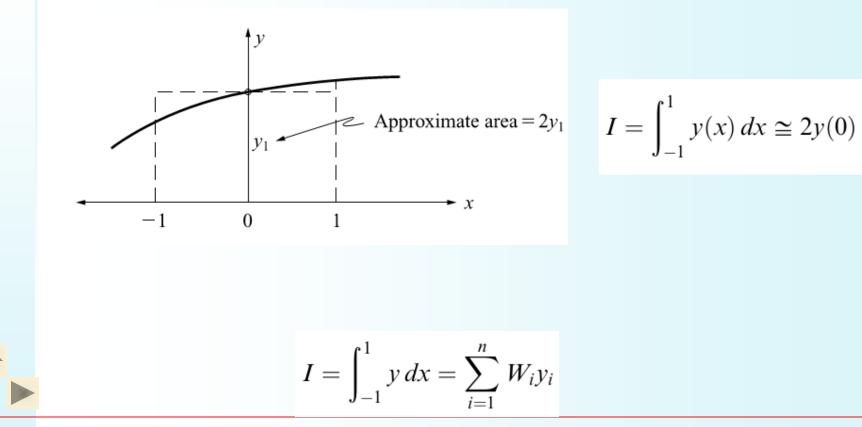


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Numerical Integration

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• Gaussian Quadrature: most useful for finite element work (evaluation of definite integrals)



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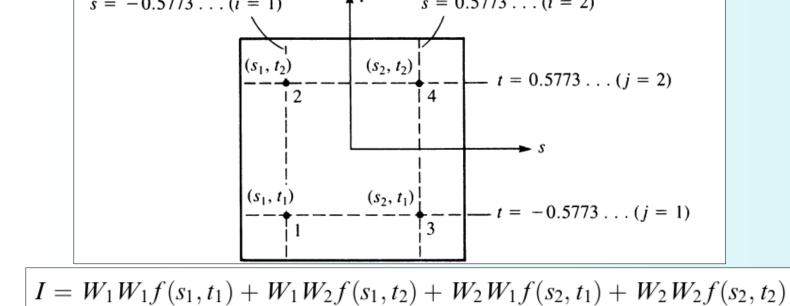


Table 10-1 Table for Gauss points for integration from minus one to one, $\int_{-1}^{1} y(x) \, dx = \sum_{i=1}^{n} W_i y_i$ Number Associated Locations, x_i of Points Weights, W_i $x_1 = 0.000 \dots$ 2.0001 2 $x_1, x_2 = \pm 0.57735026918962$ 1.0003 $\frac{5}{9} = 0.555\ldots$ $x_1, x_3 = \pm 0.77459666924148$ $\frac{8}{9} = 0.888 \dots$ $x_2 = 0.000 \dots$ $x_1, x_4 = \pm 0.8611363116$ 0.3478548451 4 $x_2, x_3 = \pm 0.3399810436$ 0.6521451549





• In two dimensions:
$$I = \int_{-1}^{1} \int_{-1}^{1} f(s,t) \, ds \, dt = \int_{-1}^{1} \left[\sum_{i} W_{i} f(s_{i},t) \right] dt$$
$$= \sum_{j} W_{j} \left[\sum_{i} W_{i} f(s_{i},t_{j}) \right] = \sum_{i} \sum_{j} W_{i} W_{j} f(s_{i},t_{j})$$



Stiffness Matrix: Gaussian

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$$\underline{k} = \int_{-1}^{1} \int_{-1}^{1} \underline{B}^{T}(s,t) \underline{D}\underline{B}(s,t) |\underline{J}| h \, ds \, dt$$

$$\underline{k} = \underline{B}^{T}(s_{1}, t_{1})\underline{D}\underline{B}(s_{1}, t_{1})|\underline{J}(s_{1}, t_{1})|hW_{1}W_{1}$$

$$+ \underline{B}^{T}(s_{2}, t_{2})\underline{D}\underline{B}(s_{2}, t_{2})|\underline{J}(s_{2}, t_{2})|hW_{2}W_{2}$$

$$+ \underline{B}^{T}(s_{3}, t_{3})\underline{D}\underline{B}(s_{3}, t_{3})|\underline{J}(s_{3}, t_{3})|hW_{3}W_{3}$$

$$+ \underline{B}^{T}(s_{4}, t_{4})\underline{D}\underline{B}(s_{4}, t_{4})|\underline{J}(s_{4}, t_{4})|hW_{4}W_{4}$$

where $s_1 = t_1 = -0.5773$, $s_2 = -0.5773$, $t_2 = 0.5773$, $s_3 = 0.5773$, $t_3 = -0.5773$, and $s_4 = t_4 = 0.5773$ as shown in Figure 10–9, and $W_1 = W_2 = W_3 = W_4 = 1.000$.

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Example 10.4: p.471

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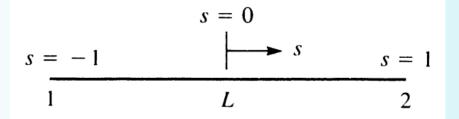
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Higher-order elements

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Linear bar element



 $N_1 = \frac{1-s}{2}$ $N_2 = \frac{1+s}{2}$

Quadratic bar element

$$N_1 = \frac{s(s-1)}{2}$$
 $N_2 = \frac{s(s+1)}{2}$ $N_3 = (1-s^2)$

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$$\{\varepsilon_x\} = \frac{du}{dx} = \frac{du}{ds}\frac{ds}{dx} = [B] \begin{cases} u_1 \\ u_2 \\ u_3 \end{cases} dx/ds = L/2 = [J]$$

$$\{\varepsilon_x\} = \frac{du}{dx} = \begin{bmatrix} \frac{2s-1}{L} & \frac{2s+1}{L} & \frac{-4s}{L} \end{bmatrix} \begin{cases} u_1\\ u_2\\ u_3 \end{cases} = \begin{bmatrix} B \end{bmatrix} \begin{cases} u_1\\ u_2\\ u_3 \end{cases}$$

$$[B] = \begin{bmatrix} \frac{2s-1}{L} & \frac{2s+1}{L} & \frac{-4s}{L} \end{bmatrix}$$

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Exercise



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- 10.8
- 10.15b
- 10.16a,e,f
- 10.18a

