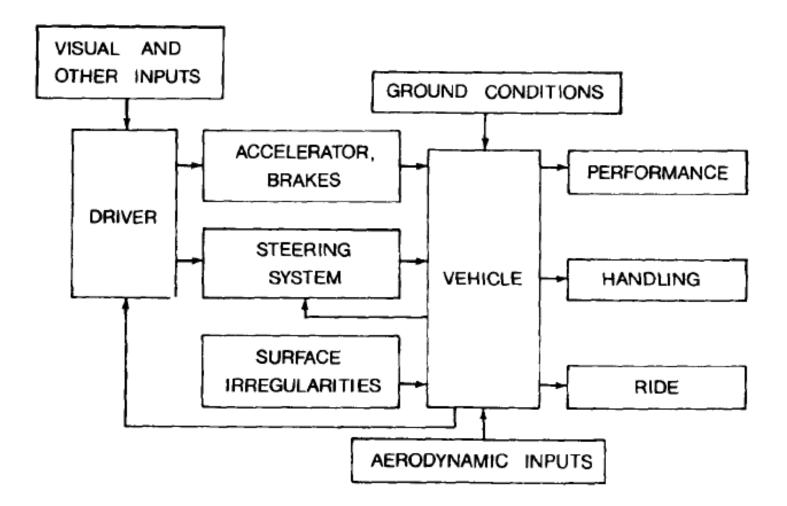


سیستمهای شاسی و بدنه خودرو چرخ و تایر

دوره کارشناسی ارشد مهندسی خودرو دانشگاه علم و صنعت ایران

پاييز ۹۵

#### Wheels and Tires



#### Wheels and Tires

Road vehicle wheels include three element

- Rim
- Tire
- Pressurized air



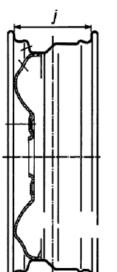
When a tire is installed on a rim and is inflated, it is called a wheel.

Vehicle wheels have two functions:

- Support the weight of the vehicle
- Exchange longitudinal and side forces with the road surface, to move the vehicle and control its path

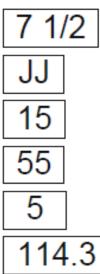
- A rim has two main parts: flange and spider. The flange (hub) is the ring or shell on which the tire is mounted. The spider (center section) is the disc section that is attached to the hub.
- Rim shape and dimensions are standardized to be exchangeable with those of other manufacturers.
- Rim size may be written as:

$$5\frac{1}{2}J \times 15$$

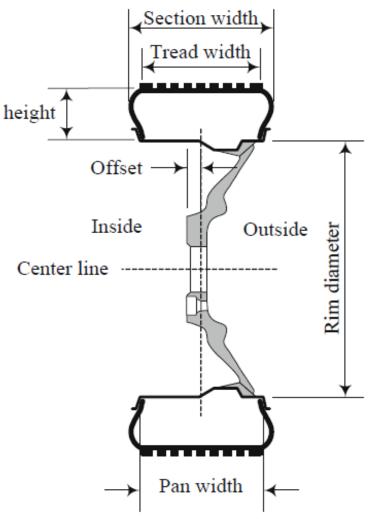


 Another sample of rim numbering and its meaning is shown below:

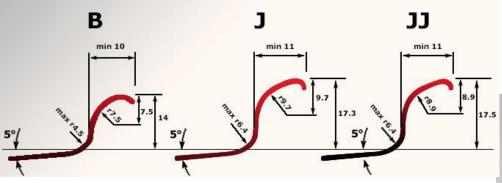
 $7\frac{1}{2} - JJ \times 15$  55 5 - 114.3



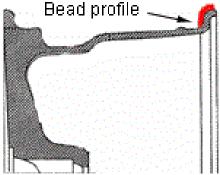
Rim width [in] Flange shape code Rim diameter [in] Offset [mm] Number of bolts Pitch circle diameter

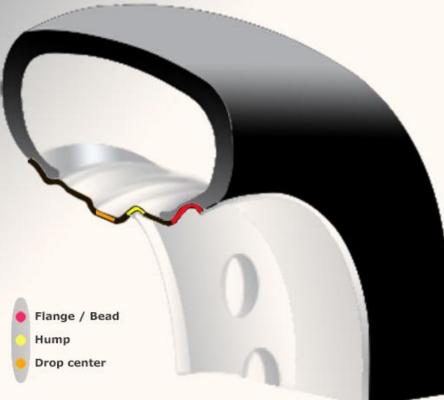


**Rim Contours or Bead Profiles** 

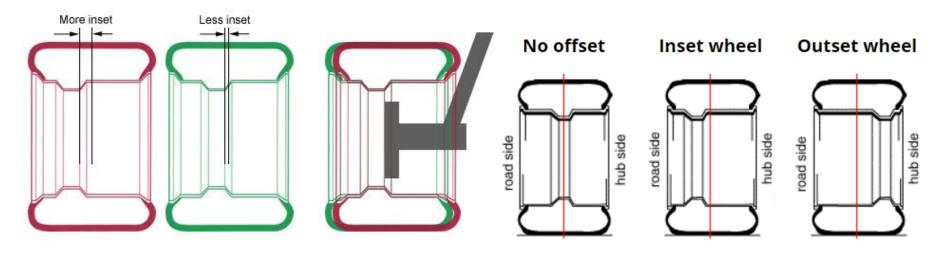


- The flange shape (bead profile) code signifies the tire-side profile of the rim and can be B, C, D, E, F, G, J, JJ, and K.
- J is the most common shape of a rim flange on passenger cars.
- B was used for smaller wheel sizes primarily for older car models
- JJ designation is most common on 4x4 and SUV vehicles.





- Offset is the distance between the inner plane and the center plane of the rim. A rim may be designed with a negative, zero, or positive offset.
- A rim has a **positive offset** if the spider is outward from the center plane (inset wheel), the wheel is tucked into the car.
- A rim has a negative offset if the spider is inward from the center plane toward the hub (outset wheel), the wheel sticks out.
- Increasing the inset of a wheel, decreases the clearance between the inner edge of the wheel and the suspension components!

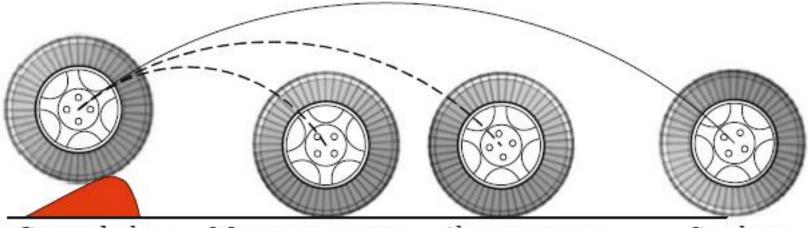


#### Pitch Circle Diameter

- The PCD, or Pitch Circle Diameter is the diameter of the invisible circle formed by scribing a circle that passes through the center point of each mounting hole (red circle in the image).
- If you've got the right number of bolts, but they're the wrong spacing, again the wheel won't fit.

### Alloy Rims

- Steel is the main material for manufacturing rims. Other than steel, composite materials and light alloys such as aluminum, magnesium, and titanium are also used for manufacturing rims.
- Weight, cost, corrosion resistance, thermal conductivity, cast-ability, machinability, recycling, and resilience are important factors in selecting rim materials.



Ground plane Magnesium rim Aluminum rim Steel rim

The difference between aluminum, magnesium, and steel rims in resilience results in the different behaviors in regaining road contact after a jump.

#### Alloy Rims

- Aluminum is very good for its weight, thermal conductivity, corrosion resistance, easy casting, low temperature, machinability, and recycling.
- Magnesium is about 30% lighter than aluminum, and is excellent for size stability and impact resistance. However, magnesium is more expensive and it is used mainly for luxury or racing cars. The corrosion resistance of magnesium is not as good as aluminum.
- Titanium is much stronger than aluminum and magnesium with excellent corrosion resistance. However, titanium is expensive and hard to be machine processed.

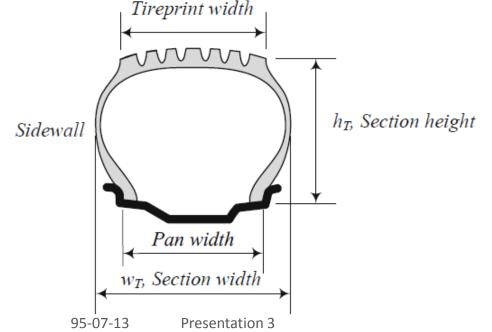




95-07-13 Presentation 3



- Average tire life is between 30,000 and 160,000 km
- Tires can be punctured and require immediate substitution.
- Tire parameters such as dimensions, maximum load carrying capacity, and maximum speed index are usually indicated on its sidewall.
- The cross section view, below, of a tire on a rim shows the dimension parameters.

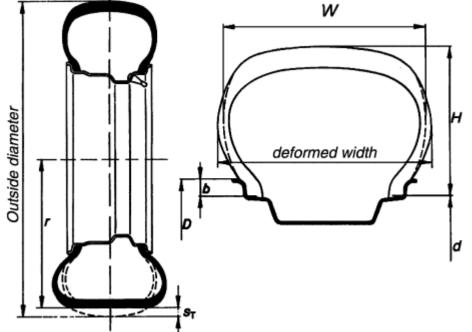


Each tire is designated by a group of letters and numbers: 185/65 R 14 82 T

- non-deformed width W
- aspect ratio (H/W)
- type of tire plies
- rim diameter
- load factor



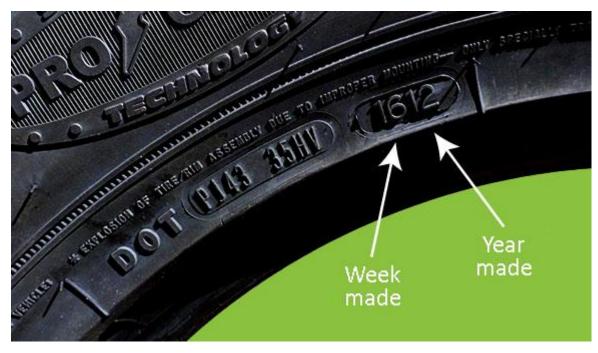
Speed $(km/h)$	80	130	150	160	170	180	190	210	240	270
Letter	$\mathbf{F}$	Μ	Р	Q	R	$\mathbf{S}$	Т	Η	V	W
			95-07-13	Pres	sentation 3					12



• The load index is a representation of the maximum load each tire is designed to support.

Index	Maximum load	84	$500  \mathrm{kg} \approx 1102  \mathrm{lbf}$	100	$800  \mathrm{kg} \approx 1764  \mathrm{lbf}$	116	$1250  \mathrm{kg} \approx 2806  \mathrm{lbf}$
0	$45  \mathrm{kg} pprox 99  \mathrm{lbf}$	85	$515 \mathrm{kg} \approx 1135 \mathrm{lbf}$	101	$825 \mathrm{kg} pprox 1819 \mathrm{lbf}$	117	$1285  \text{kg} \approx 2833  \text{lbf}$
		86	$530  \mathrm{kg} \approx 1163  \mathrm{lbf}$	102	$850  \mathrm{kg} pprox 1874  \mathrm{lbf}$	118	$1320 \mathrm{kg} \approx 2910 \mathrm{lbf}$
71	$345\mathrm{kg}pprox761\mathrm{lbf}$	87	$545 \mathrm{kg} \approx 1201 \mathrm{lbf}$	103	$875  \mathrm{kg} pprox 1929  \mathrm{lbf}$	119	$1360 \mathrm{kg} \approx 3074 \mathrm{lbf}$
72	$355  \mathrm{kg} pprox 783  \mathrm{lbf}$	88	$560  \mathrm{kg} \approx 1235  \mathrm{lbf}$	104	$900  \mathrm{kg} \approx 1984  \mathrm{lbf}$	120	$1400 \text{ kg} \approx 3086 \text{ lbf}$
73	$365  \mathrm{kg} pprox 805  \mathrm{lbf}$	89	$580  \mathrm{kg} \approx 1279  \mathrm{lbf}$	105	$925\mathrm{kg}pprox 2039\mathrm{lbf}$	121	$1450 \text{ kg} \approx 3197 \text{ lbf}$
74	$375 \mathrm{kg} pprox 827 \mathrm{lbf}$	90	$600  \mathrm{kg} \approx 1323  \mathrm{lbf}$	106	$950\mathrm{kg}pprox 2094\mathrm{lbf}$	122	$1500 \text{ kg} \approx 3368 \text{ lbf}$
75	$387  \mathrm{kg} \approx 853  \mathrm{lbf}$	91	$615  \mathrm{kg} \approx 1356  \mathrm{lbf}$	107	$975\mathrm{kg}pprox 2149\mathrm{lbf}$	123	$1550 \text{ kg} \approx 3417 \text{ lbf}$
76	$400  \mathrm{kg} \approx 882  \mathrm{lbf}$	92	$630  \text{kg} \approx 1389  \text{lbf}$	108	$1000  \mathrm{kg} \approx 2205  \mathrm{lbf}$	124	$1600 \text{ kg} \approx 3527 \text{ lbf}$
77	$412  \mathrm{kg} \approx 908  \mathrm{lbf}$	93	$650  \mathrm{kg} \approx 1433  \mathrm{lbf}$	109	$1030\mathrm{kg} \approx 2271\mathrm{lbf}$	124	$1650 \text{ kg} \approx 3690 \text{ lbf}$
78	$425  \mathrm{kg} \approx 937  \mathrm{lbf}$	94	$670  \mathrm{kg} \approx 1477  \mathrm{lbf}$	110	$1060  \mathrm{kg} \approx 2337  \mathrm{lbf}$		0
79	$437  \mathrm{kg} \approx 963  \mathrm{lbf}$	95	$690  \text{kg} \approx 1521  \text{lbf}$	111	$1090  \mathrm{kg} \approx 2403  \mathrm{lbf}$	126	$1700 \text{ kg} \approx 3748 \text{ lbf}$
80	$450 \mathrm{kg} \approx 992 \mathrm{lbf}$	96	$710 \mathrm{kg} \approx 1565 \mathrm{lbf}$	113	$1120  \mathrm{kg} \approx 2469  \mathrm{lbf}$	127	$1750 \mathrm{kg} \approx 3858 \mathrm{lbf}$
81	$462 \text{ kg} \approx 1019 \text{ lbf}$	97	$730 \mathrm{kg} \approx 1609 \mathrm{lbf}$	113	$1150  \mathrm{kg} \approx 2581  \mathrm{lbf}$	128	$1800  \mathrm{kg} \approx 3968  \mathrm{lbf}$
82	$475 \text{ kg} \approx 1047 \text{ lbf}$	98	$750 \text{ kg} \approx 1653 \text{ lbf}$	114	$1180 \mathrm{kg} \approx 2601 \mathrm{lbf}$		
83	$487 \mathrm{kg} \approx 1074 \mathrm{lbf}$	99	$775 \mathrm{kg} \approx 1709 \mathrm{lbf}$	115	$1215  \mathrm{kg} pprox 2679  \mathrm{lbf}$	199	$13600 \mathrm{kg} \approx 30000 \mathrm{lbf}$

• The manufacturing date of a tire is indicated on the tire sidewall using four digits representing the week and year the tire was built, e.g. 1612 represents week #16 of year 2012.



#### Uniform Tire Quality Grading (UTQG)

Tire manufacturers also rate their products for wear, wet traction, and heat resistance.

• Tread wear rating index: The higher the wear number, the longer the tire lifetime. An index of 100 is equivalent to approximately 20000 miles or 32000km.

Index	Life (Approximate)				
100	$32000\mathrm{km}$	20000 mi			
150	$48000\mathrm{km}$	30000 mi			
200	$64000\mathrm{km}$	40000 mi			
250	$80000\mathrm{km}$	50000 mi			
300	$96000\mathrm{km}$	60000 mi			
400	129000 km	80000 mi			
500	161000 km	100000 mi			

#### Uniform Tire Quality Grading (UTQG)

- Wet traction: wet traction is rated in letters between "A" to "C" where A is the best, B is intermediate and C is acceptable. An A wet traction rating is typically an indication that the tire has a deep open tread pattern with lots of fine lines in the tread blocks.
- Heat resistance: heat resistance is rated in letters between "A" to "C", where A is the best. An A heat resistance rating indicates two things: first, low rolling resistance due to stiffer tread belts, stiffer sidewalls, or harder compounds; second, thinner sidewalls and more stable blocks in the tread pattern.

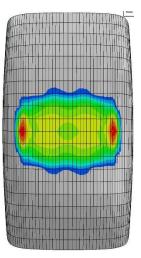
#### Uniform Tire Quality Grading (UTQG)

- Temperature rating: is indicated by a letter between "A" to "C", where A is the best.
- Traction rating: indicates how well a tire grips the road surface. This is an overall rating for both dry and wet conditions. Tires are rated as: "AA" for the best, "A" for better, "B" for good, and "C" for acceptable.



#### Tireprint (tire footprint, contact patch)

- The contact area between a tire and the road is called the tireprint. At any point of a tireprint, the normal and friction forces are transmitted between the road and tire.
- The effect of the contact forces can be described by a resulting force system including force and torque vectors applied at the center of the tireprint.
- The area of the tireprint is inversely proportional to the tire pressure.
- Lowering the tire pressure is a technique used for off-road vehicles in sandy, muddy, or snowy areas, and for drag racing.





#### **Proper Inflation Pressure**

- In a properly-inflated tire, approximately 95% of the vehicle weight is supported by the air pressure in the tire and 5% is supported by the tire wall.
- An under-inflated tire will support less of the vehicle weight with the air pressure in the tire; therefore, more weight will be supported by the tire wall. This tire load increase causes the tire to have a larger tireprint that creates more friction and more heat.
- In an over-inflated tire, too much of the vehicle weight is supported by the tire air pressure. The vehicle will be bouncy and hard to steer because the tireprint is small and only the center of the tireprint is contacting the road.

## Plus one (+1) concept

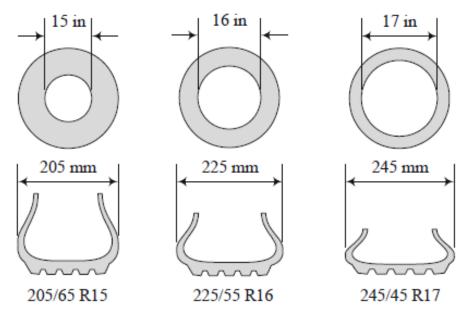
- Speedometer is calibrated to tell the speed by how many times the wheel spins around.
- If you make your wheel diameter smaller, it's going to spin more times to go the same distance.
- Your car doesn't know you changed the tire and wheel size, so it will give you an inaccurate reading.
- Plus one (+1) concept is used to put wider, bigger wheels and tires on cars without sacrificing speedometer accuracy.

#### Plus one (+1) concept



#### Use online calculators (may give different results) OR Use the following procedure

### Plus one (+1) concept



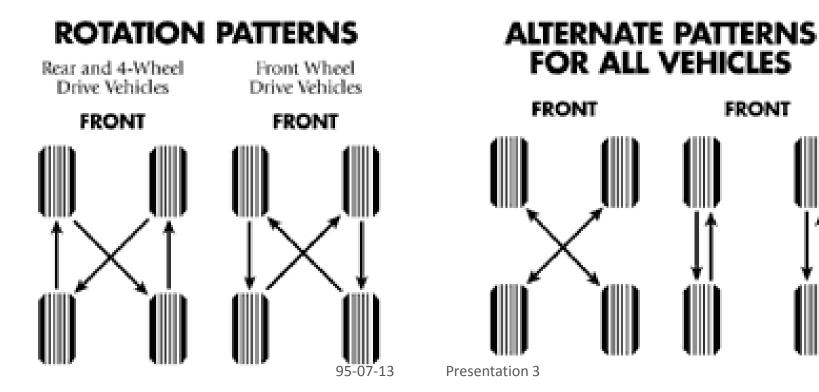
- add 20mm to the tire width
- subtract 10% from the aspect ratio.
- add 1 in to the rim diameter,

#### Rim width

- aspect ratio of 50 and above
- 70% of the tire's width, rounded to the nearest 0.5 in
- 255/50R16 tire width of 255mm = 10.04 in \* 70% = 7.028 ≈ 7 in [7 x 16 rim] (up to 8.5 in wide).
- aspect ratio of 45 and below
- 85% of the tire's width, rounded to the nearest 0.5 in
- 255/45R17 tire width of 255mm = 10.04 in \* 85% = 8.534 in≈ 8.5in [8 ½ x 17 rim] (up to 10 in wide).
- A rim width of up to 1.5 inch wider can also be used.

#### Rotating the tires

- In most vehicles, the front and rear tires will wear at different rates. So, it ٠ is advised to swap the front and rear tires as they wear down to even out the wear patterns.
- Front tires, especially on front-wheel drive vehicles, wear out more quickly • than rear tires.



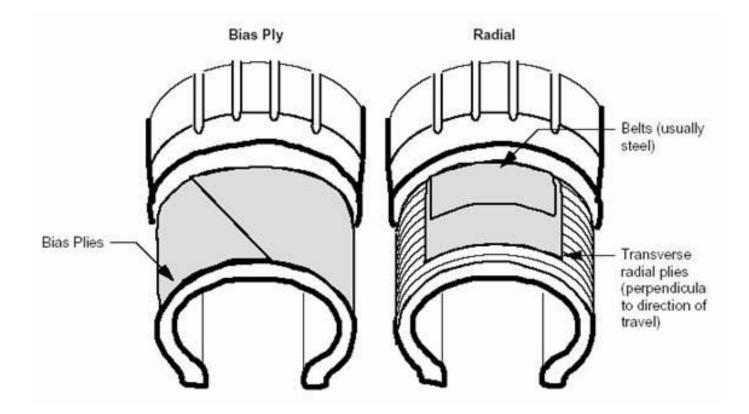
FRONT

#### Wheels and Tires

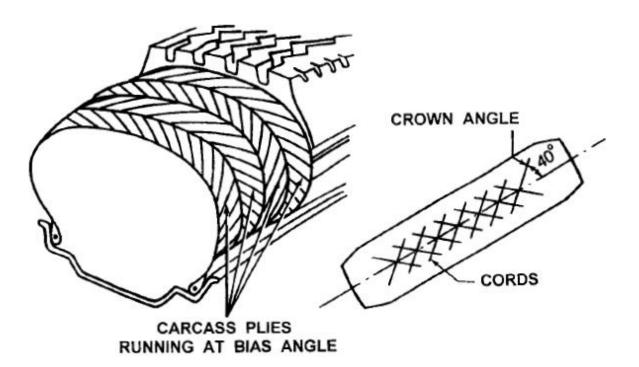
The average weight of a passenger car tire is 10-12 kg. The average weight of a light truck tire is 14-16 kg. The average weight of commercial truck tire is 135-180 kg.



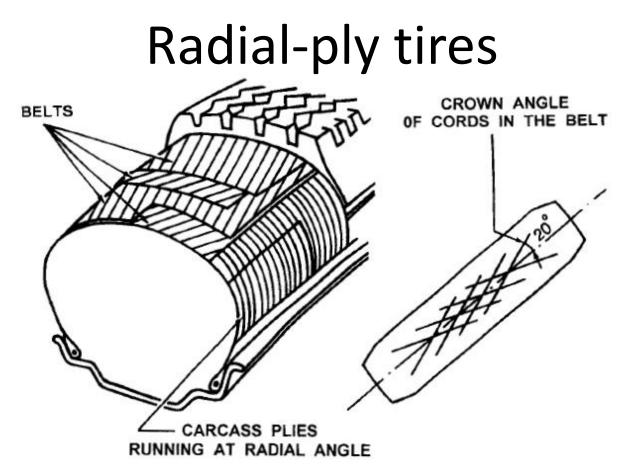
#### **Tire Structure**



#### Cross-ply (bias) tires



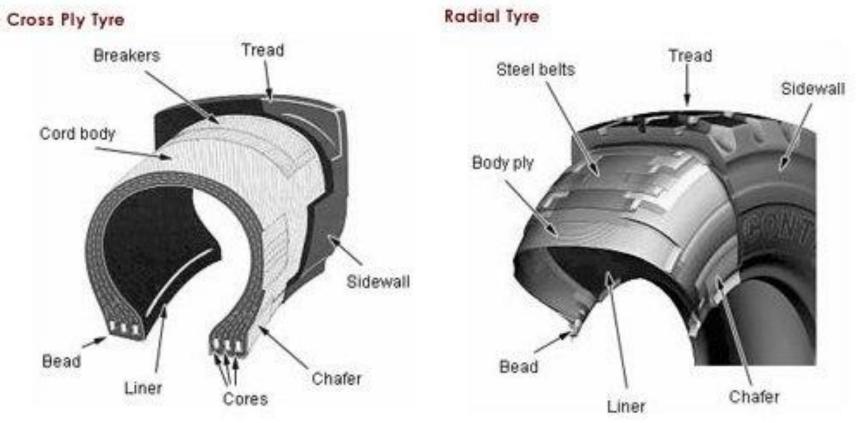
A bias-ply tire has two plies (for light-load tires) or more (up to 20 plies for heavy-load tires). The cords in adjacent plies overlap in a diamond-shaped (criss-cross) pattern.



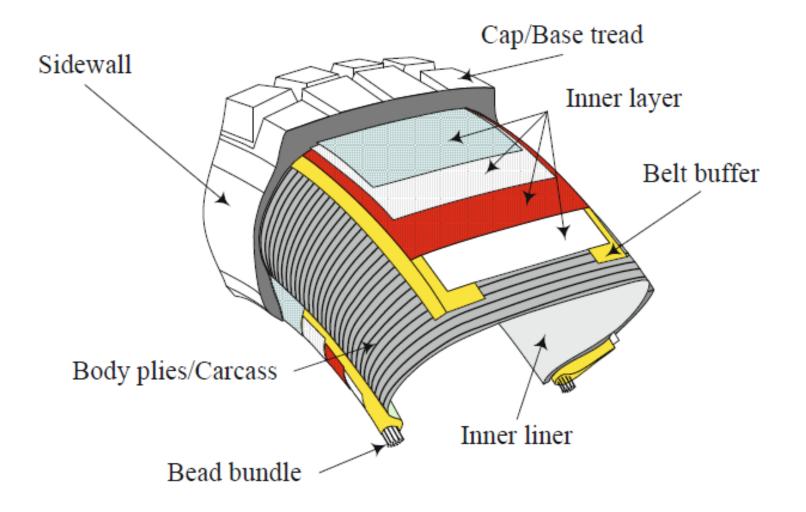
A radial-ply tire has one or more layers of cords in the carcass extending radially from bead to bead, resulting in a crown angle of 90°. A belt of several layers of cords (usually steel or other high-modulus materials) is fitted under the tread. The cords in the belt are laid at a low crown angle of approximately 20°.

For passenger car tires, usually there are two radial plies in the carcass and two plies of steel cords and two plies of synthetic material cords in the belt. For truck tires, usually there is one radial steel ply in the carcass and four steel plies in the belt.

#### **Tire Structure**



The strength of bias-ply tires increases by increasing the number of plies and bead wires. However, more plies means more mass, which increases heat and reduces tire life. To increase a radial tire's strength, larger diameter steel cables are used in the tire's carcass.



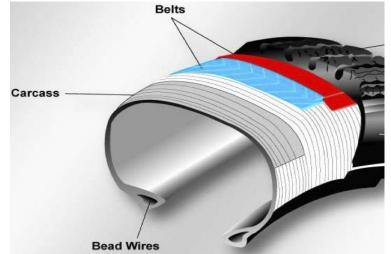
 Bead or bead bundle is a loop of high strength steel cable coated with rubber. It gives the tire the strength it needs to stay seated on the wheel rim and to transfer the tire forces to the

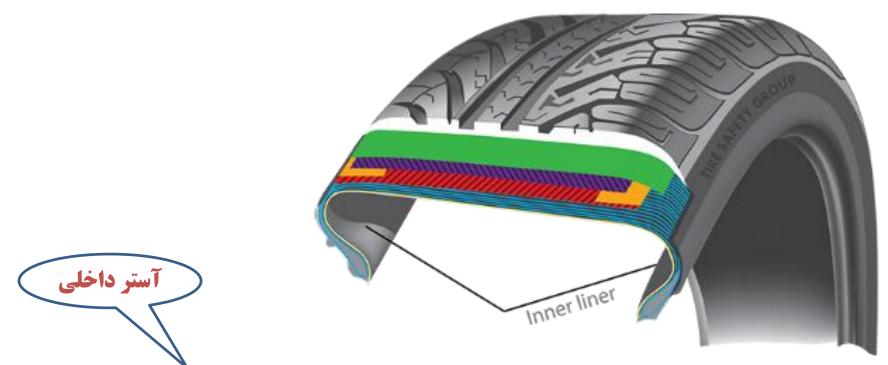
rim.

طوقه



- Inner layers also called plies are made up of different fabrics. The most common ply cords are cotton, polyester, rayon, steel, fiberglass, and aramid.
- The carcass composed of the body plies, keep the air in the tire and are the main part in supporting the tension forces generated by tire air pressure.
- A tire's strength is often described by the number of carcass plies or the thickness of the ply cords.





 An inner liner is a specially compounded rubber that forms the inside of a tubeless tire, which prevents loss of air pressure.

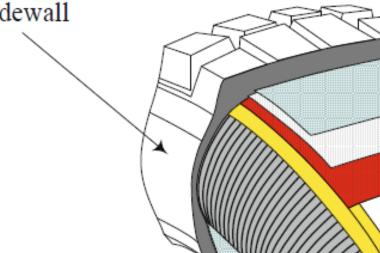
Aam

 Belts are rubber-coated layers of steel, polyester, nylon, Kevlar or other materials running around the tire circumference, under the tread. They are designed to reinforce body plies to hold the tread flat on the road and make the best contact with the road.



دیوارہ تایر

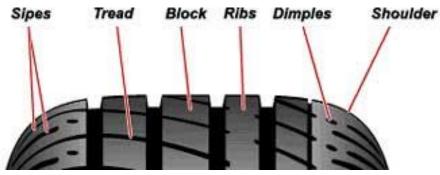
 The sidewall provides lateral stability for the tire and protects the body plies. It may contain additional components to help increase the lateral stability.



# آج تاير

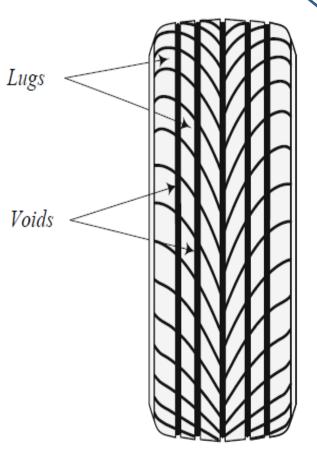
شیا، های

- The tread is the portion of the tire that comes in contact with the road. The tread is made from a mixture of different kinds of natural and synthetic rubbers.
- Tread designs vary widely depending on the specific purpose of the tire. The tread groove is the space or area between two tread rows or blocks. The tread groove gives the tire traction and is especially useful dring rain or snow.



# **Tire Components**

شیار ها



The tread pattern is made up of lugs (blocks) and voids (grooves). The lugs are the sections of rubber that make contact with the road and voids are the spaces that are located between the lugs.

- Wide and straight grooves running circumferentially have a lower noise level and high lateral friction.
- Lateral grooves running from side to side increase traction and noise levels.
- Tires need both circumferential and lateral grooves.
   The water on the road is compressed into the grooves by the vehicle's weight and is evacuated from the tireprint region, out to the sides of the wheel.
- Self-cleaning is the ability of a tire's tread pattern to release mud or material from the voids. A better mud tire releases the mud or material easily from the voids.

# Tire Components

There are five major rubbers used in tire production:

- natural rubber,
- stirene-butadiene rubber (SBR),
- butadiene rubber (BR),
- butyl rubber,
- halogenated butyl rubber.

The first three are primarily used for tread and sidewall compounds, while butyl rubber and halogenated butyl rubber are primarily used for the inner liner and the inside portion that holds the compressed air inside the tire.

Η

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H

H - C - H

— *C* –

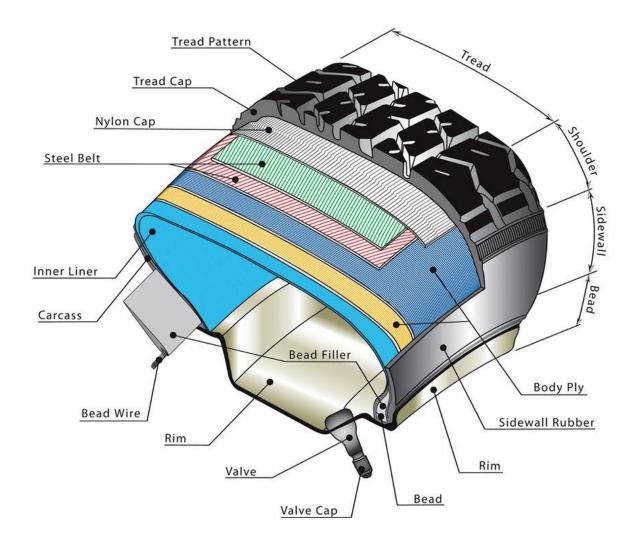
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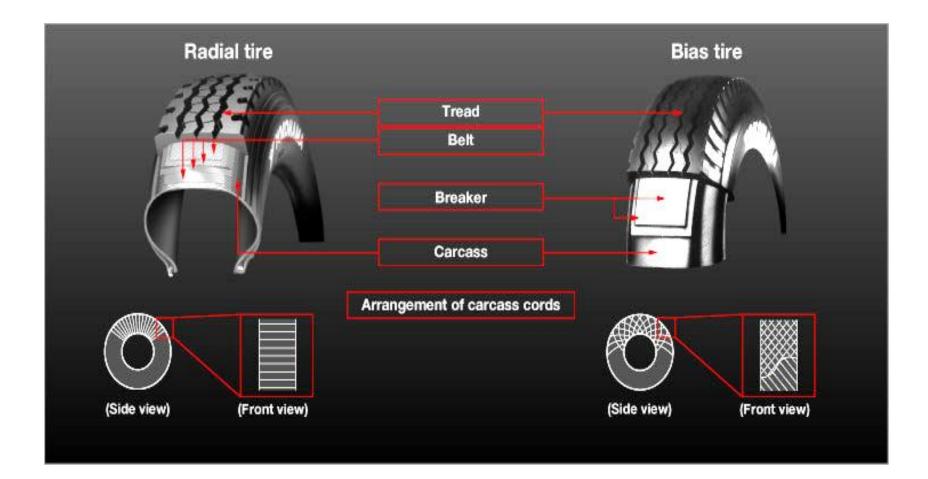
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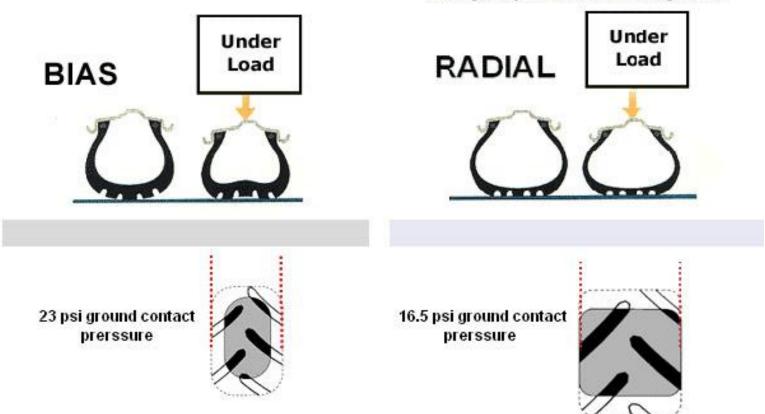
#### **Tire Components**



#### **Tire Structure**



### **Tire Structure**

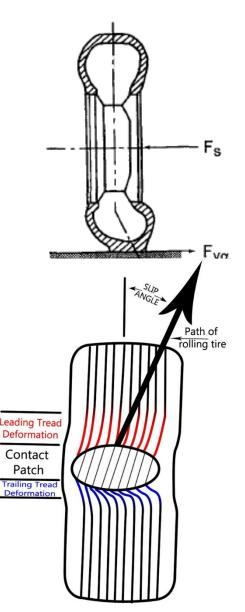


The lugs stay in contact with the ground.

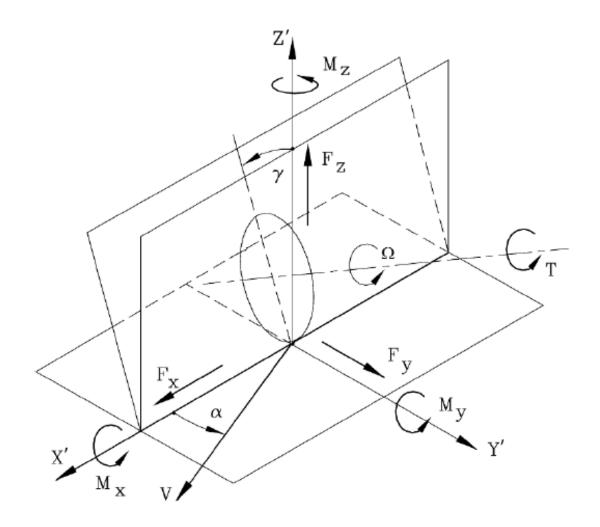
# Wheels and Tires

- Rubber is the main material used to make a tire compliant. The elastic characteristic of a tire allows the tire to be pointed in a direction different than the direction the car is pointed.
- There is no way for a vehicle to turn without rubber tires, unless it moves at a very low speed.





#### Wheels and Tires



# Wheels and Tires

• Wheel sideslip angle  $\alpha$ 

angle between the X'Z' plane and the direction of the wheel hub

• Inclination or camber angle γ

angle between the X'Z' plane and the wheel equatorial plane

- While the inclination angle is stated with reference to the road, the camber angle is usually stated with reference to the car
- We will assume that inclination and camber angle coincide

# **Tire Operation**

- Prepared ground, when the tire is in contact with paved or concrete surfaces (on-road driving)
- Unprepared ground, when the tire is in contact with natural surfaces or dirt roads (off-road driving)
- The physical phenomenon discriminating the two:
- Ground deformation is neglected on dry paved roads.
- Ground deformations should be considered in unprepared roads.

Two different aspects of on-road driving are considered:

- The *adhesion between rubber and ground; because of this phenomenon,* tires can exchange forces with the ground.
- The elasticity of the tire structure; gives the tire the capabilities to absorb certain road irregularities.
- These are the primary reasons that tires slip in two directions of the area of contact when longitudinal and lateral forces are applied.

Rubber-ground adhesion

 the result of physical phenomena that allow a specimen of rubber set on the ground and pressed with a certain vertical force to withstand forces contained in the ground plane, without any relative motion.

Adhesion is caused by two phenomena:

- Physical adhesion
- Local deformation

Physical adhesion

- Attraction forces between rubber molecules and ground molecules (between adhesive sites)
- Impurities present between the two contact surfaces
- Lateral forces are balanced by the adhesion force

Adhesion force is controlled by:

- Surface energy of contacting materials.
- Damping properties of those materials (especially rubber); controlled by temperatures and relative speed.
- Deformation of contacting surfaces, because of lateral forces which can also cause instability as in the case of stick and slip.

Local deformations

• caused by road irregularities

- Adhesion force comprises about 70% of the total friction force when rubber is on dry paved road.
- These phenomena change their mechanism radically on wet surfaces;

Three fundamental cases:

- Water layer thickness is high enough to establish a permanent lubricated opening between tire and ground (aquaplaning); (tangential forces can be calculated from liquid viscosity).
- Water layer thickness is insufficient to establish permanent lubrication, but sufficient to preclude adhesion forces; local deformation forces can still occur if the ground is rough.
- Water is completely removed from the contact area. The behavior of rubber is then as was explained (by means of tire grooves and draining pavement).

- Ground deformations should also be taken into account
- Ground deformations could predominate in certain situations, which can interfere with the mechanical parts of the chassis.

Shape of the surface has a purely geometric impact on chassis design, concerning:

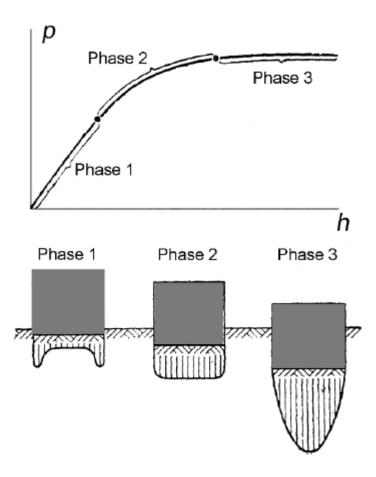
- Wheelbase
- Track
- Wheel diameter
- Available suspension stroke
- Clearance of the chassis from the ground and
- Attack angles

• The mechanical properties of soil are determined by the solid incoherent particles that are its main component;

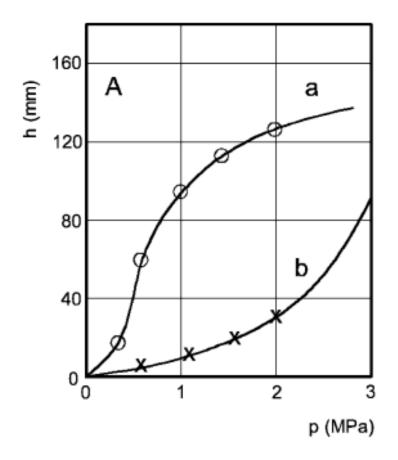
The primary characteristics of these particles are:

- granulometry,
- apparent density (*apparent* vs *real* density)
- water content (*humidity*) expressed in percent of water to solids
- *liquid limit:* cohesive effect between particles and therefore the shear resistance of the soil is eliminated
- plastic limit: the soil looses its capability of being shaped, being too brittle
- *plasticity index:* difference between the two limits
- *relative content of water of the soil:* ratio between the actual water content of a given soil and the quantity related to the plastic limit

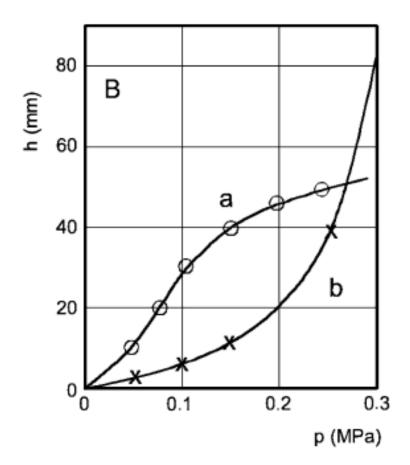
sinking h as a function of applied pressure p, for various kinds of soil



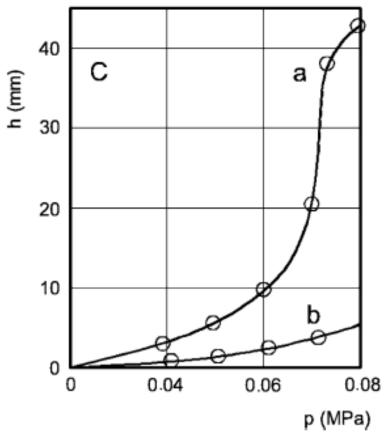
• Cohesive soil (a: humid soil, b: plastic soil);



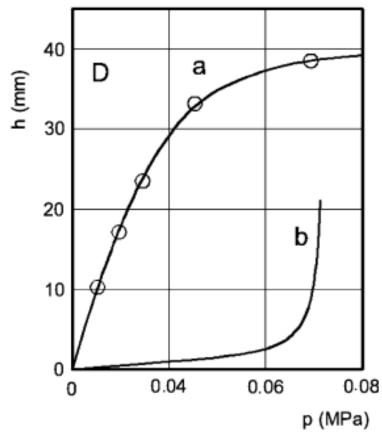
• Sandy soil (a: loose sand, about 200 mm thick; b: a compacted layer);



Layer of peat (a: pressing pad of 4 m<sup>2</sup> of surface; b: pressing pad of about 0.4 m<sup>2</sup>);



Snowy ground (a: fresh snow, density of 0.15 g/cm<sup>2</sup>, b: compacted snow, density of 0.20 g/cm<sup>2</sup>).



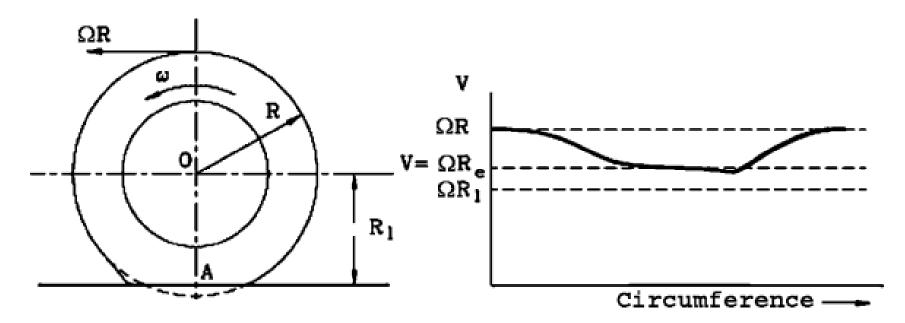
# **Rolling Radius**

• Relationship between the angular velocity Ω and the forward speed V of a rolling rigid wheel of radius R is simply:

 $V = \Omega R$ 

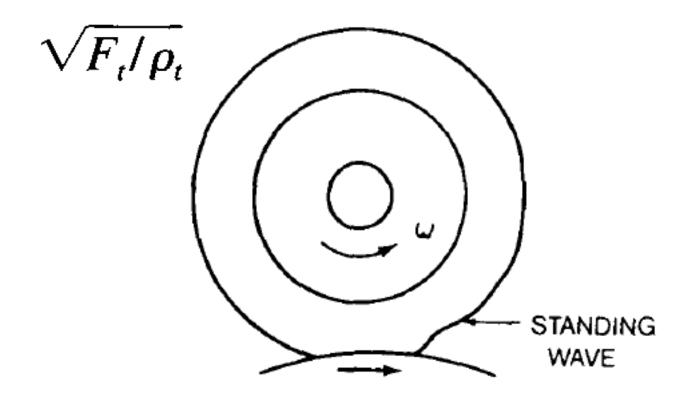
• for a pneumatic tire an effective rolling radius *Re can be defined:* 

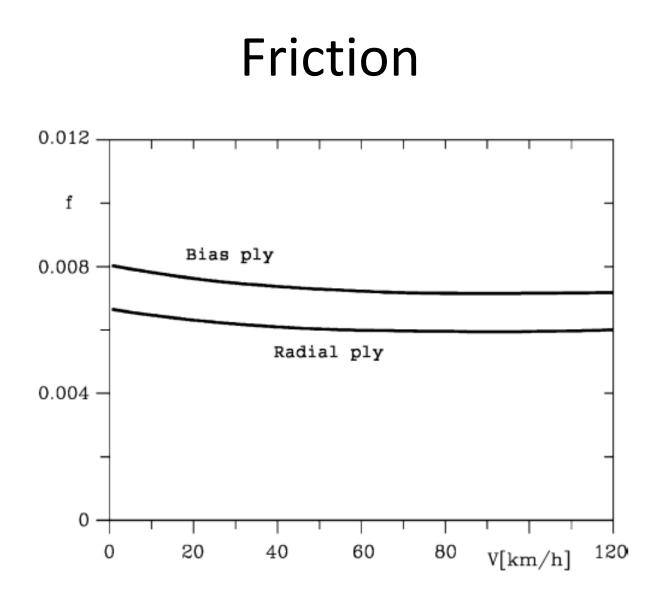
 $Re = V/\Omega$ 



### **Standing Waves**

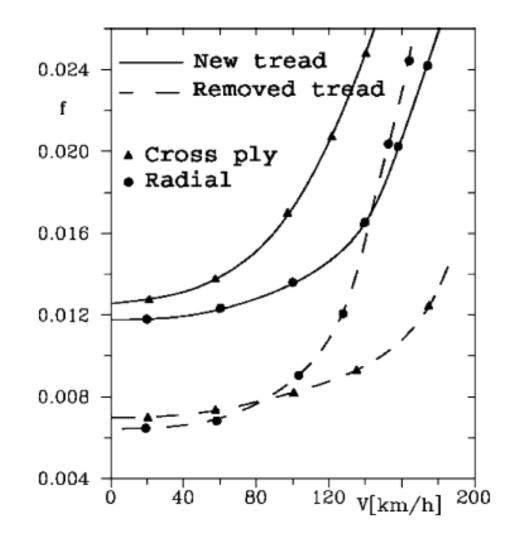
Formation of Standing Waves at Threshold Speed





95-07-22 Presentation 5

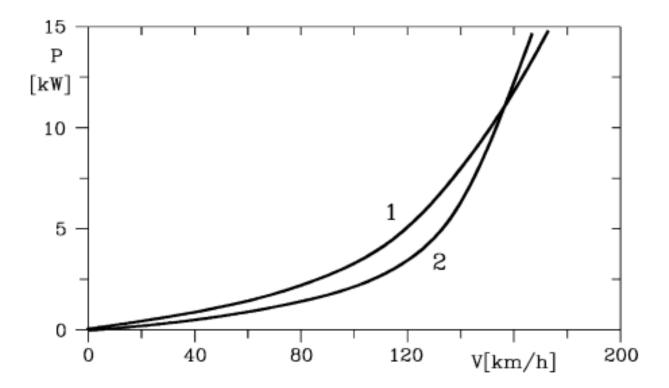
#### Effect of wear on friction



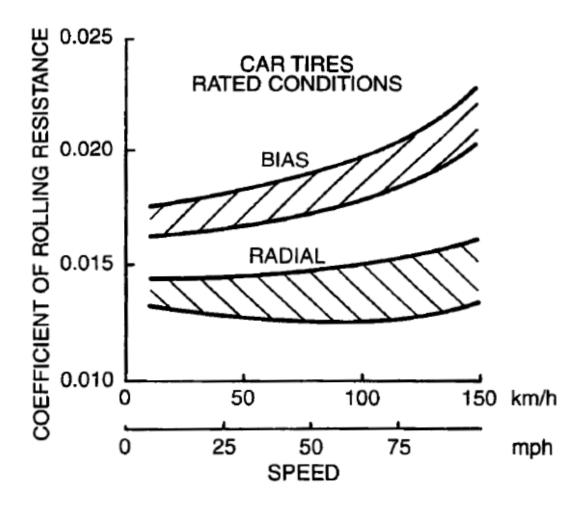
95-07-22 Presentation 5

### **Rolling Power**

Rolling power as a function of speed. Curve 1: synthetic rubber; curve 2: natural rubber.

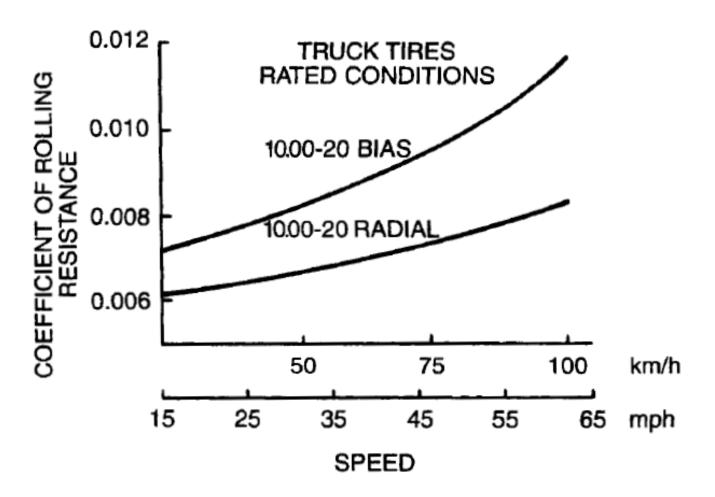


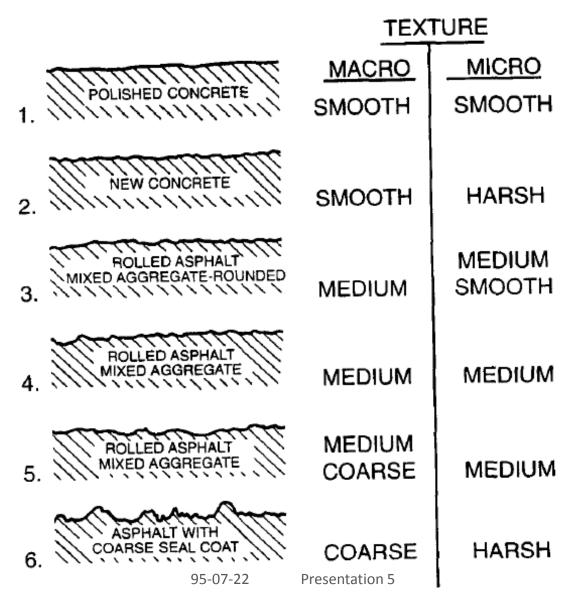
Smooth, flat road surface under rated load and inflation pressure



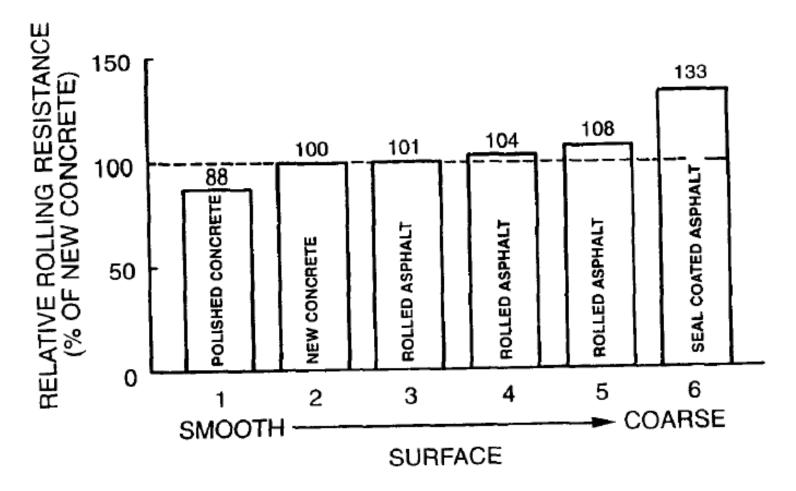
95-07-22 Presentation 5

Tires of same size under rated load and inflation pressure

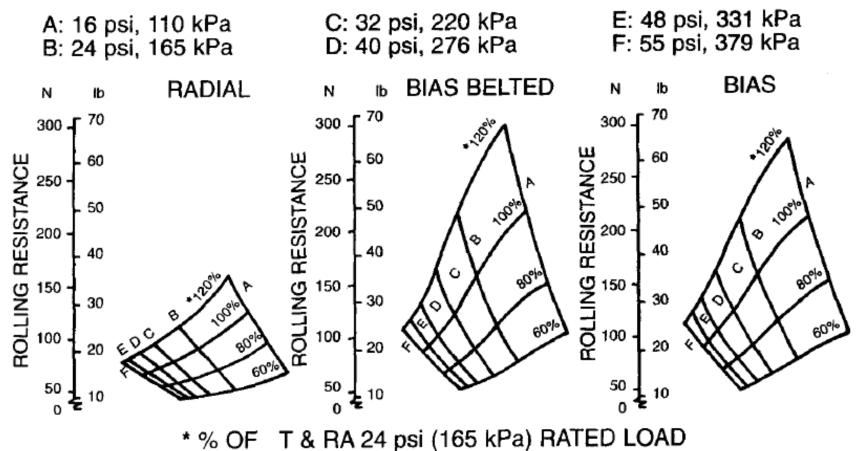




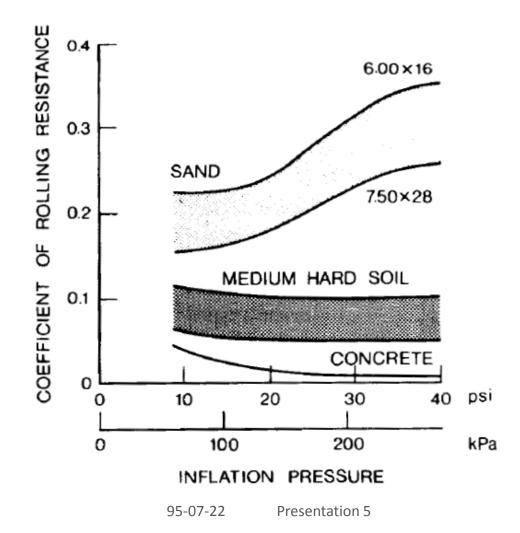




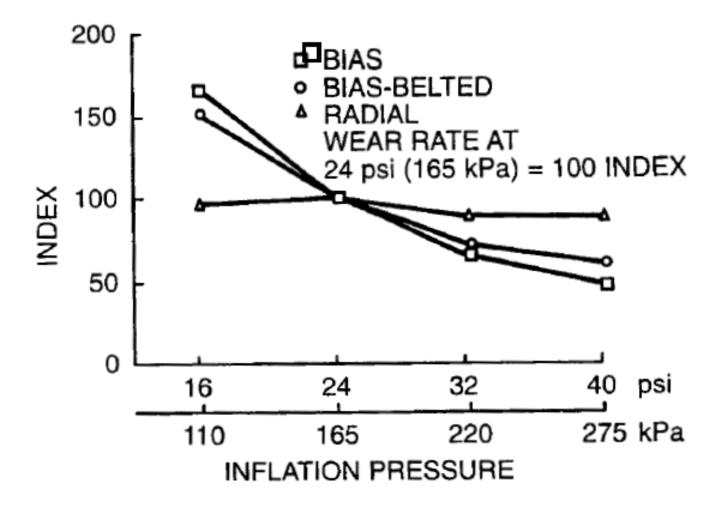
Variation of rolling resistance of radial-ply, bias-belted, and bias-ply car tires with load and inflation pressure



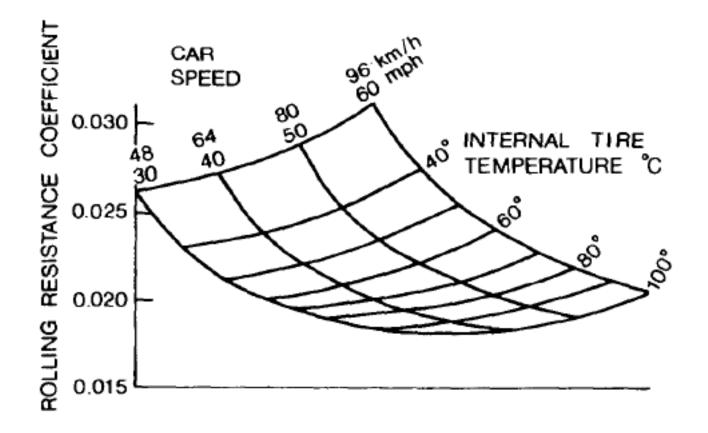
Variation of rolling resistance of types of deformable ground with inflation pressure



**Tread Wear** 



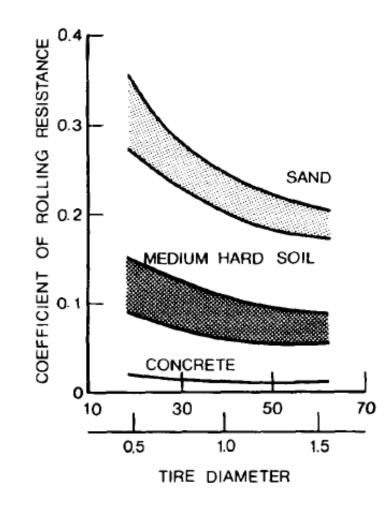
Car tire



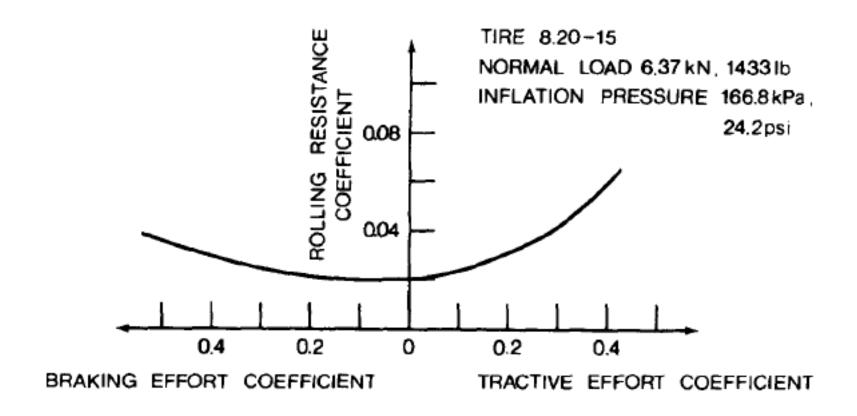
Car tire

0.030 COEFFICIEN' 728 lb, 3238 N 970 lb, 4314 N 0.025 1213 lb, 5395 N 0.020 ROLLING RESISTANCE 0.015 0.010 0.005 80 °C -20 20 0 40 60 SHOULDER TEMPERATURE

Car tire



Truck tire



# **Coefficient of Rolling Resistance**

#### **Empirical formulas**

radial-ply passenger car tires

$$f_r = 0.0136 + 0.40 \times 10^{-7} V^2$$

bias-ply passenger car tires

$$f_r = 0.0169 + 0.19 \times 10^{-6} V^2$$

radial-ply truck tires

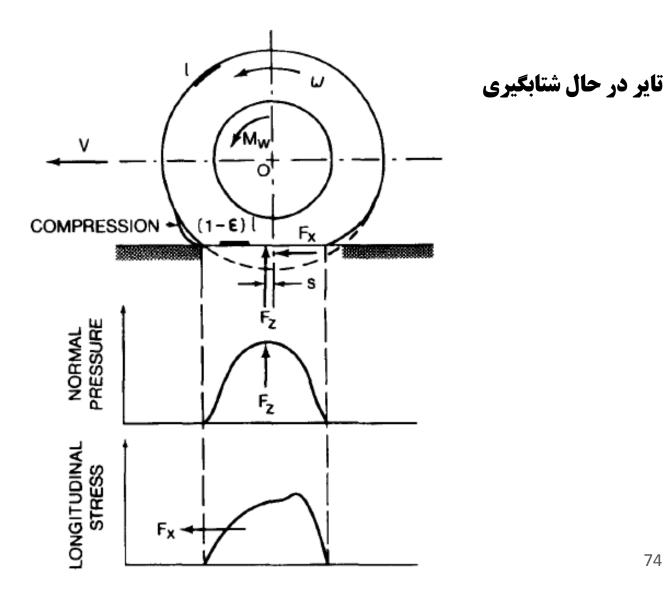
$$f_r = 0.006 + 0.23 \times 10^{-6} V^2$$

bias-ply truck tires

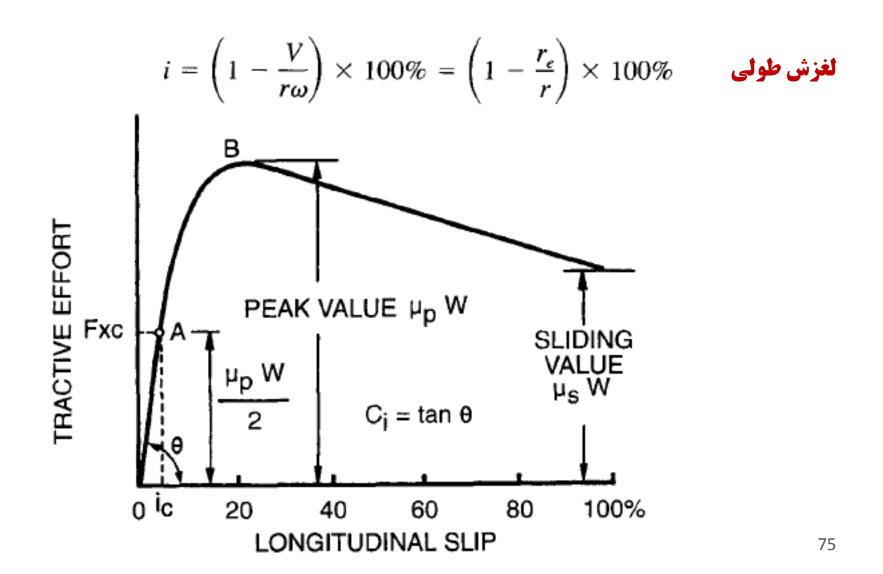
$$f_r = 0.007 + 0.45 \times 10^{-6} V^2$$

V is in km/h

73



74



تغییر شکل طولی در 
$$e = e_0 + x\epsilon$$
طول سطح تماس

تغییر شکل طولی در  $e_0 = \lambda \epsilon$  ایتدای سطح تماس

$$e = (\lambda + x)\epsilon$$

نیروی طولی دیفرانسیلی 
$$rac{dF_x}{dx} = k_t e = k_t (\lambda + x) oldsymbol{\epsilon}$$
 بر واحد طول المان

برآیند نیروی طولی 
$$F_x = \int_0^x k_t (\lambda + x) \epsilon \ dx = k_t \lambda x \epsilon \left( 1 + \frac{x}{2\lambda} \right)$$

تئوري اصلي (Julien)

تئوري اصلي (Julien)

$$\begin{split} F_x &= \int_0^x k_t (\lambda + x) \epsilon \, dx = k_t \lambda x \epsilon \left( 1 + \frac{x}{2\lambda} \right) & \text{integral} \\ F_x &= k_t \lambda l_t \epsilon \left( 1 + \frac{l_t}{2\lambda} \right) = K_t \epsilon \\ x &\leq l_c = \frac{\mu_p p b}{k_t \epsilon} - \lambda = \frac{\mu_p W}{l_t k_t \epsilon} - \lambda \end{split}$$

$$l_{t} = l_{c} = \frac{\mu_{p}W}{l_{t}k_{t}i} - \lambda$$
$$i_{c} = \frac{\mu_{p}W}{l_{t}k_{t}(l_{t} + \lambda)}$$
$$F_{xc} = \frac{\mu_{p}W[1 + (l_{t}/2\lambda)]}{1 + (l_{t}/\lambda)}$$

لبه انتهایی سطح تماس در آستانه لغزش

Presentation 3

$$F_{xs} = \mu_p W(1 - l_c/l_t)$$
 در ناحیه غیرخطی

$$F_{xa} = k_t \lambda i l_c \left( 1 + \frac{l_c}{2\lambda} \right)$$

$$F_x = F_{xs} + F_{xa} = \mu_p W - \frac{\lambda (\mu_p W - K'i)^2}{2l_t K'i} \qquad K' = l_t k_t \lambda$$

مشخص کردن مقدار پارامتر λ در این تئوری نیاز، زحمت زیادی دارد و باید با انجام اندازه گیری های دقیقی صورت گیرد.

تئوری ساده سازی شده با صرف نظر از ۸

در فاحیه خطی  
در فاحیه خطی  

$$K_t = k_t x \epsilon = k_t x i$$
 $F_x = \int_0^{l_t} k_t ix \, dx = (k_t l_t^2/2) i$ 
 $\frac{k_t l_t^2}{2} = C_i = \tan \theta = \frac{\partial F_x}{\partial i} \Big|_{i=0}$ 
 $F_x = C_i i$ 

تئوری ساده سازی شده با صرف نظر از λ

آستانه لغزش 
$$\frac{dF_x}{l_t} = k_t l_t i = \mu_p p b = \frac{\mu_p W}{l_t}$$
 بر واحد طول المان

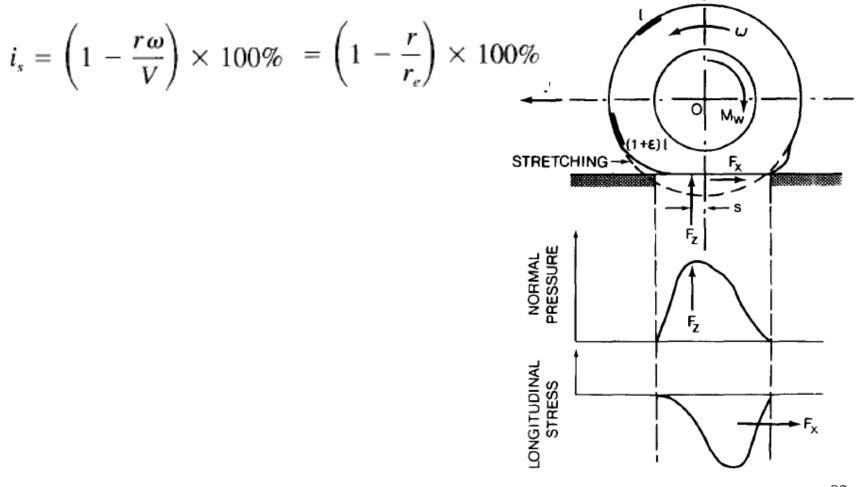
$$i_c = \frac{\mu_p W}{k_t l_t^2} = \frac{\mu_p W}{2C_i}$$
$$F_{xc} = C_i i_c = \frac{\mu_p W}{2}$$

تئوری ساده سازی شده با صرف نظر از λ

$$F_x = F_{xs} + F_{xa} = \mu_p W \left( 1 - \frac{\mu_p W}{4C_i i} \right)$$

# **Braking Effort**

تئوری ساده سازی شده (برای تایر در ترمزگیری)



95-07-13 Presentation 3

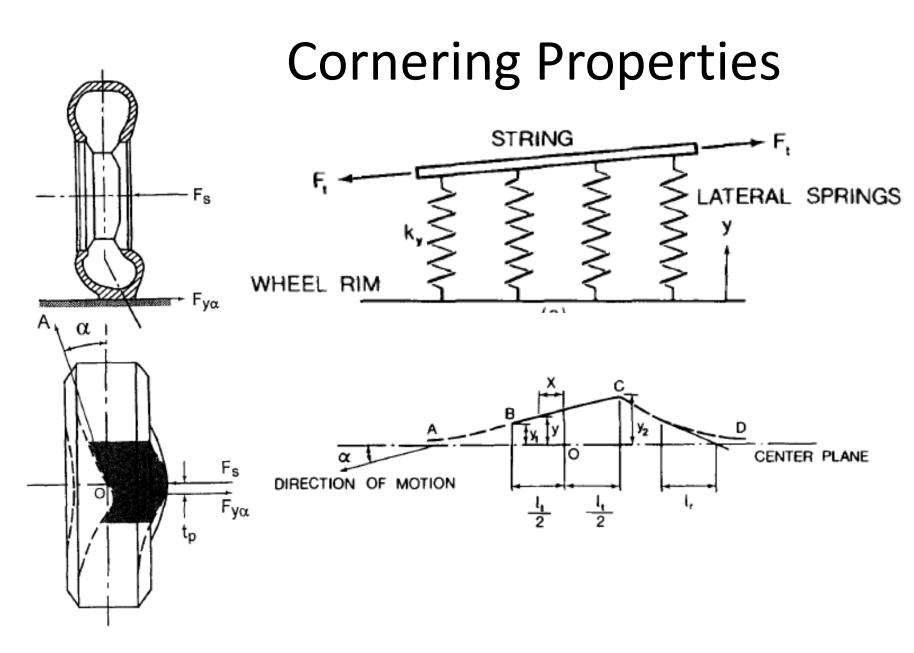
## **Braking Effort**

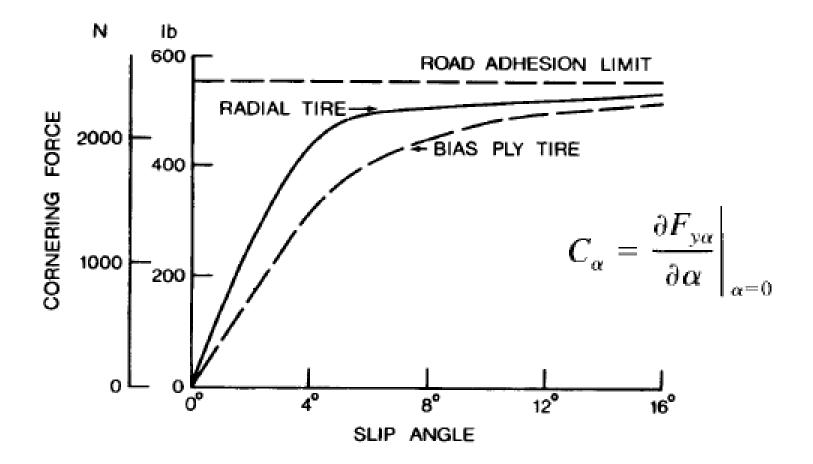
تئوری ساده سازی شده (برای تایر در ترمزگیری)

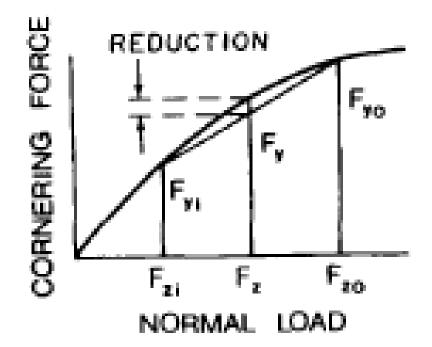
$$|i| = |i_s/(1 - i_s)|$$
  
 $F_x = C_s i_s/(1 - i_s)$ 
 $C_s = \frac{\partial F_x}{\partial i_s}\Big|_{i_s=0}$ 

$$i_{sc} = \frac{\mu_p W}{2C_s + \mu_p W}$$
  $F_{sc} = \frac{C_s i_{sc}}{1 - i_{sc}} = \frac{\mu_p W}{2}$ 

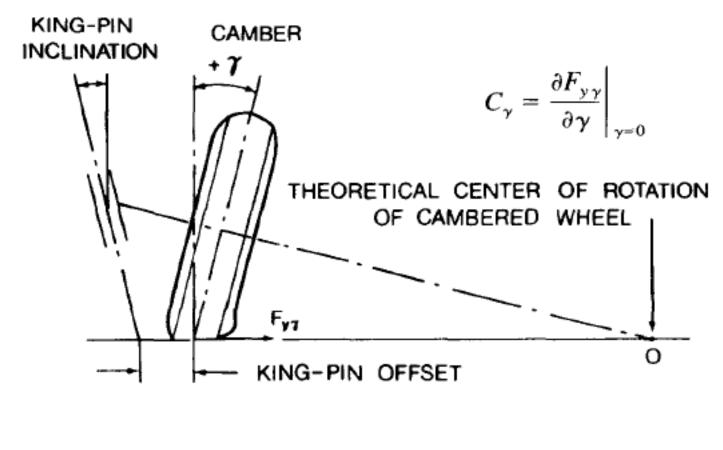
$$F_x = \mu_p W \left[ 1 - \frac{\mu_p W (1 - i_s)}{4C_s i_s} \right]$$
 بالغزش







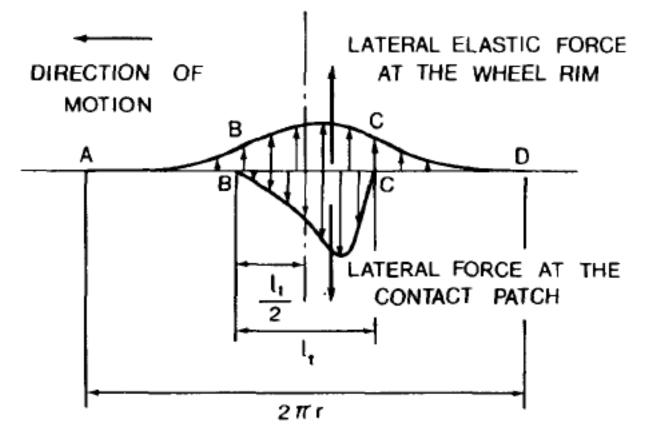
### **Camber Thrust**



 $F_y = F_{y\alpha} \pm F_{y\gamma}$   $F_y = C_{\alpha}\alpha \pm C_{\gamma}\gamma$ 

$$dF_{y1} = k_y y \ dx \qquad \text{options} \text{ for } x = k_y y \ dx \qquad \text{options} \text{ for } y = k_y y \ dx \qquad \text{options} \text{ for } y = k_y y \ dx \qquad \text{options} \text{ for } y = k_y \left[ \frac{d^2 y}{dx^2} \ dx \qquad \text{options} (x + d \exists y) \right] = 0 \qquad \text{for } x = d \exists y \ dx = k_y \left[ \frac{d^2 y}{dx^2} \right] = 0 \qquad \text{for } y = y_2 \ \text{sinh} \left[ (x - l_t/2)/l_r \right] + y_1 \ \text{sinh} \left[ (l_t/2 + l_h - x)/l_r \right] \qquad \text{for } x > l_t/2 \qquad \text{for } x > l_t/2 \qquad \text{for } y = y_1 \ \text{exp} \left[ \frac{-(x - l_t/2)}{l_r} \right] \qquad x > l_t/2 \qquad x > l_t/2 \qquad \text{for } x > l_t/2 + l_h \qquad y = y_2 \ \text{exp} \left[ \frac{-(l_t/2 + l_h - x)}{l_r} \right] \qquad x < l_t/2 + l_h \qquad \text{for } x > l_t/2 + l_h \qquad y = y_2 \ \text{exp} \left[ \frac{-(l_t/2 + l_h - x)}{l_r} \right] \qquad x < l_t/2 + l_h \qquad x < l_t/2 = l_t \ \text{for } x < l_t/2 + l_h \qquad x < l_t/2 + l_h \qquad x < l_t/2 = l_t \ \text{for } x < l_t/2 + l_h \qquad x < l_t \ \text{for } x < l_t/2 + l_h \qquad x < l_t \ \text{for } x < l_t/2 + l_h \qquad x < l_t \ \text{for } x < l_t/2 + l_h \qquad x < l_t/2 + l_h \qquad x < l_t \ \text{for } x < l_t/2 + l_h \qquad x < l_t \ \text{for } x < l_t/2 + l_h \qquad x < l_t/2 + l_h \qquad x < l_t \ \text{for } x < l_t/2 + l_h \qquad x < l_t \ \text{for } x < l_t \ \text{for } x < l_t \ \text{for } x < l_t/2 + l_h \qquad x < l_t \ \text{for } x < l_t \ \text{for }$$

CENTERLINE



$$\begin{split} \frac{\text{Temple}}{\text{Temple}} k_y \left( y - l_r^2 \frac{d^2 y}{dx^2} \right) & \left\{ \begin{aligned} dF_{y1} &= k_y y \ dx \\ dF_{y2} &= -F_t \frac{d^2 y}{dx^2} \ dx \end{aligned} \right\} \\ \end{split}$$

نیروی عرضی تایر در سطح تماس

$$F_{y} = k_{y} \int_{-l_{t}/2}^{l_{t}/2} \left( y - l_{r}^{2} \frac{d^{2}y}{dx^{2}} \right) dx$$
  
$$= k_{y} \int_{-l_{t}/2}^{l_{t}/2} y \, dx - k_{y} l_{r}^{2} \left( \frac{dy}{dx} \right) \Big]_{-l_{t}/2}^{l_{t}/2}$$
  
$$= k_{y} \left( y_{1} + y_{2} \right) l_{t}/2 + k_{y} l_{r} \left( y_{1} + y_{2} \right)$$
  
$$= k_{y} \left( y_{1} + y_{2} \right) (l_{r} + l_{t}/2)$$

$$\frac{\text{Temple}}{dk_y}\left(y-l_r^2\frac{d^2y}{dx^2}\right) - \begin{bmatrix} dF_{y1} = k_y y \ dx \\ dF_{y2} = -F_i \frac{d^2y}{dx^2} \ dx \end{bmatrix}$$

گشتاور نیروی عرضی تایر حول محور قائم در مرکز سطح تماس (گشتاور بازگرداننده)

$$\begin{split} M_z &= k_y \int_{-l_r/2}^{l_r/2} x \left( y - l_r^2 \frac{d^2 y}{dx^2} \right) dx \\ &= k_y \int_{-l_r/2}^{l_r/2} xy \, dx - k_y l_r^2 \left( x \frac{dy}{dx} - y \right) \Big]_{-l_r/2}^{l_r/2} \\ &= k_y \frac{(l_r/2)^2}{3} \left( y_1 - y_2 \right) + k_y l_r \left( l_r + \frac{l_r}{2} \right) \left( y_1 - y_2 \right) \\ &= k_y (y_1 - y_2) \left[ \frac{(l_r/2)^2}{3} + l_r \left( l_r + \frac{l_r}{2} \right) \right] \end{split}$$

تئورى Temple

در غیاب لغزش در سطح تماس

$$\alpha \simeq \tan \alpha = \frac{y_1 - y_2}{l_r} = -\frac{y_1}{l_r}$$

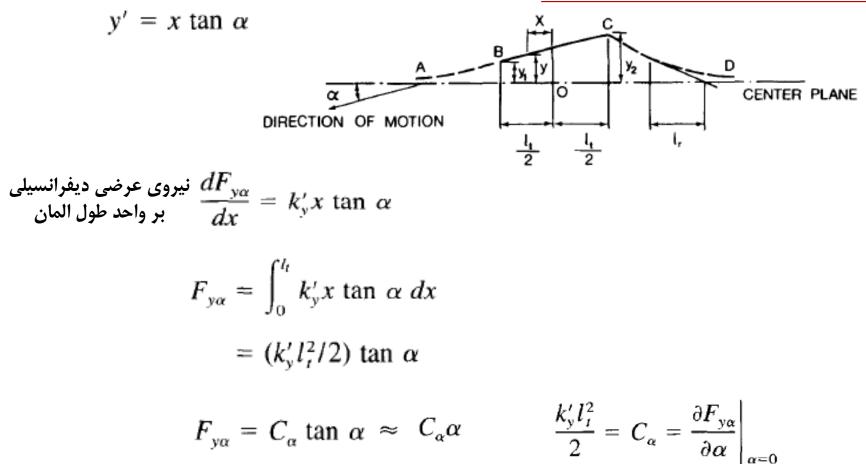
با جایگذاری این مقدار در رابطه نیروی عرضی تایر و گشتاور بازگرداننده:

$$\frac{F_y}{\alpha} = 2k_y \left(l_r + \frac{l_t}{2}\right)^2$$
$$\frac{M_z}{\alpha} = k_y l_t \left[\frac{(l_t/2)^2}{3} + l_r \left(l_r + \frac{l_t}{2}\right)\right]$$

Pneumatic trail:

$$t_p = \frac{M_z}{F_y} = \frac{(l_t/2) \left[ (l_t/2)^2 / 3 + l_r \left( l_r + l_t/2 \right) \right]}{(l_r + l_t/2)^2}$$

تئوری ساده سازی شده (در غیاب لغزش)



تئوری ساده سازی شده (آستانه لغزش)

$$\alpha_c = \frac{\mu_p W}{2C_a} \qquad \qquad F_{yac} = \frac{\mu_p W}{2}$$

با وجود لغزش

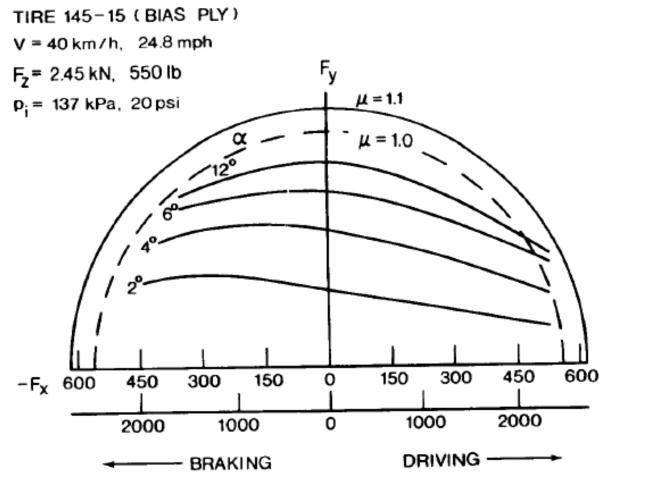
$$F_{y\alpha} = \mu_p W \left( 1 - \frac{\mu_p W}{4C_\alpha \tan \alpha} \right) = \mu_p W \left( 1 - \frac{\mu_p W}{4C_\alpha \alpha} \right)$$

**نمونه ای از روابط تجربی برای تخمین نیروهای عرضی تایر** 

$$F_{y\alpha} = c_1 \alpha + c_2 \alpha^2 + c_3 \alpha^3$$

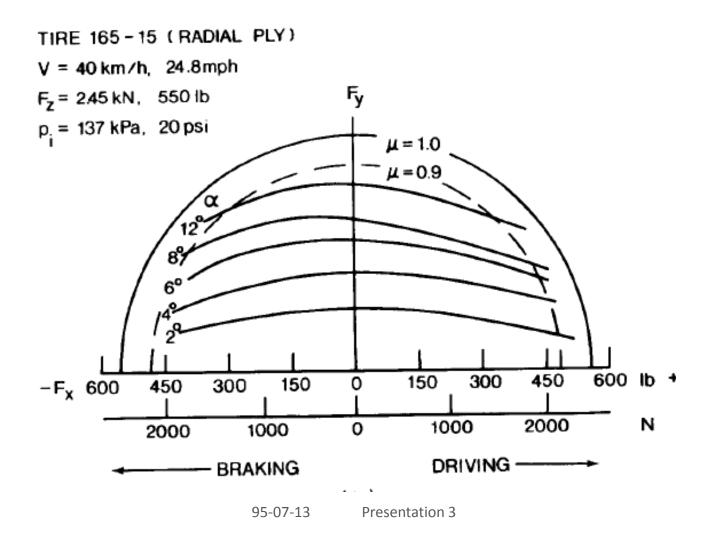
### **Friction Ellipse**

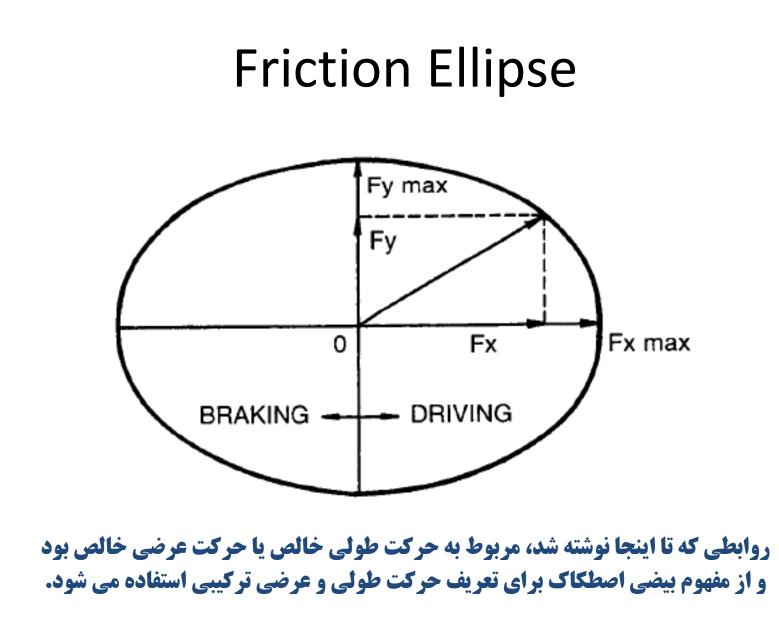
تفاوت قابلیت ایجاد نیروی عرضی تایر بایاس در شتابگیری و ترمزگیری



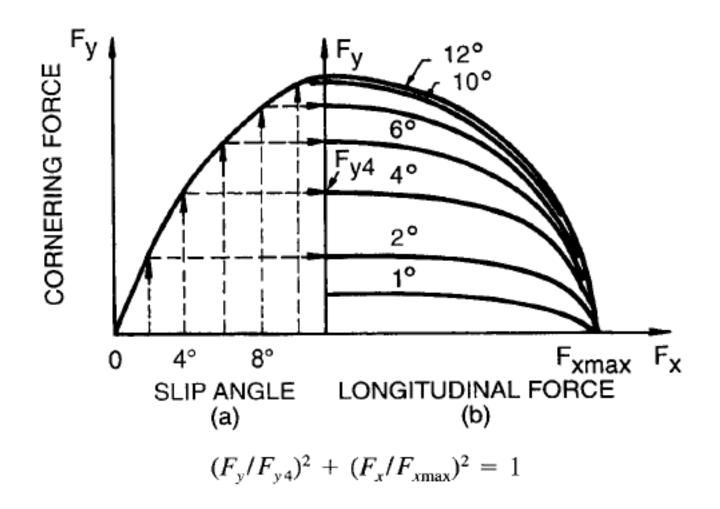
### **Friction Ellipse**

تفاوت نامحسوس قابلیت ایجاد نیروی عرضی تایر رادیال در شتابگیری و ترمزگیری





#### **Friction Ellipse**



#### **Combined Cornering and Braking**

ترکیب تئوری های ساده سازی شده حرکت طولی خالص و حرکت عرضی خالص

$$\frac{dF_x}{dx} = k_t x i_s / (1 - i_s)$$
 نبروی طولی دیفرانسیلی  $\frac{dF_x}{dx} = k_t x i_s / (1 - i_s)$  بر واحد طول المان  $y' = x \tan \alpha / (1 - i_s)$  نبروی عرضی دیفرانسیلی  $\frac{dF_{y\alpha}}{dx} = k'_y x \tan \alpha / (1 - i_s)$  نبروی عرضی دیفرانسیلی بر اساس بیضی اصطکاک، شرط عدم لغزش نقطه ای در فاصله x از جلوی سطح تماس، این است که برآیند نیروهای طولی و عرضی از اصطکاک کمتر باشند:  
 $\sqrt{[k_t x i_s / (1 - i_s)]^2 + [k'_y x \tan \alpha / (1 - i_s)]^2}} = \mu p b = \frac{\mu W}{l_t}$ 
 $J$  طول سطح تماس  $J$  طول سطح تماس  $J$  میزان است که برآیند نیروهای مرابع عرضی از اصطکاک کمتر باشند:  
 $\sqrt{[k_t x i_s / (1 - i_s)]^2 + [k'_y x \tan \alpha / (1 - i_s)]^2}}$ 

# Combined Cornering and Braking

 $\begin{aligned} \bar{t}_{c} &= \frac{\mu W(1 - i_{s})}{2\sqrt{(k_{t}l_{t}^{2}i_{s}/2)^{2} + (k_{y}'l_{t}^{2}\tan\alpha/2)^{2}}} & k_{t}l_{t}^{2}/2 = C_{s} \quad k_{y}'l_{t}^{2}/2 = C_{\alpha'} \end{aligned}$   $= \frac{\mu W(1 - i_{s})}{2\sqrt{(C_{t}i_{s})^{2} + (C_{s}\tan\alpha)^{2}}}$ 

If  $I_c / I_t \ge 1$ , the entire contact patch is an adhesion region:

$$F_{x} = \int_{0}^{t_{t}} [k_{t}xi_{s}/(1 - i_{s})] dx = k_{t}l_{t}^{2}i_{s}/2(1 - i_{s})$$
  

$$= C_{s}i_{s}/(1 - i_{s})$$
  

$$F_{y\alpha} = \int_{0}^{t_{t}} [k_{y}'x \tan \alpha/(1 - i_{s})] dx$$
  

$$= k_{y}'l_{t}^{2} \tan \alpha/2(1 - i_{s})$$
  

$$= C_{\alpha} \tan \alpha/(1 - i_{s})$$
  
Presentation 3

100

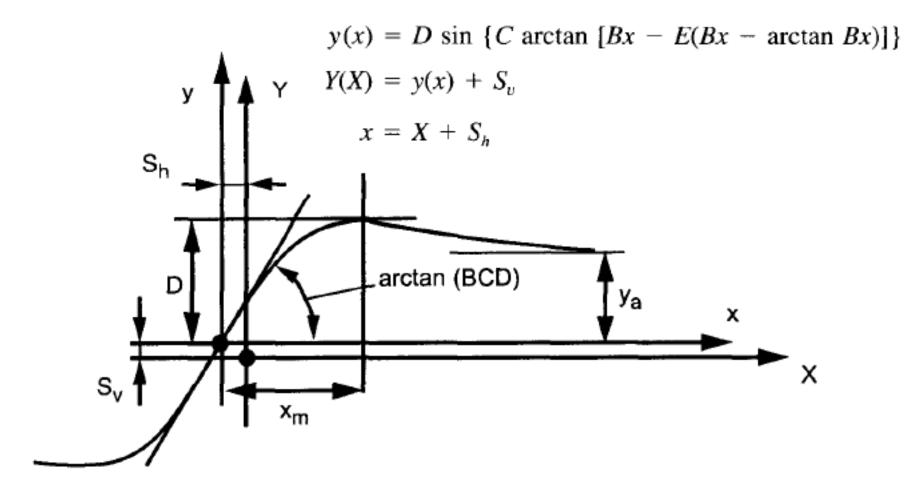
#### **Combined Cornering and Braking**

ترکیب تئوری های ساده سازی شده حرکت طولی خالص و حرکت عرضی خالص

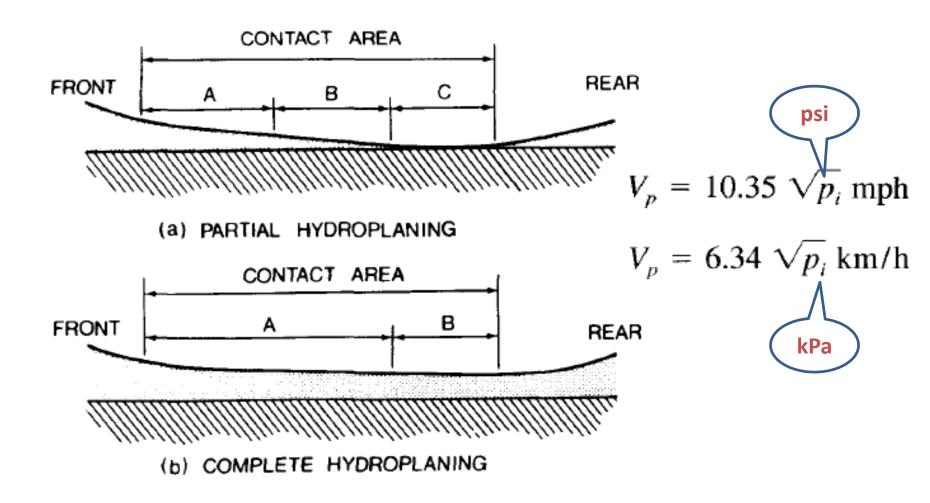
If  $I_c / I_t < 1$ , sliding between the tread and the ground will take place:

$$\begin{split} F_{xa} &= \int_{0}^{l_{c}} [k_{t}xi_{s}/(1-i_{s})] \, dx = \frac{\mu^{2}W^{2}C_{s}i_{s}(1-i_{s})}{4 \left[(C_{s}i_{s})^{2} + (C_{\alpha}\tan\alpha)^{2}\right]} \\ &= \frac{\mu WC_{s}i_{s}}{4 \left[(C_{s}i_{s})^{2} + (C_{\alpha}\tan\alpha)^{2}\right]} \left[1 - \frac{\mu W(1-i_{s})}{2\sqrt{(C_{s}i_{s})^{2} + (C_{\alpha}\tan\alpha)^{2}}}\right] \\ F_{x} &= F_{xa} + F_{xs} = \frac{\mu WC_{s}i_{s}}{\sqrt{(C_{s}i_{s})^{2} + (C_{\alpha}\tan\alpha)^{2}}} \left[1 - \frac{\mu W(1-i_{s})}{4\sqrt{(C_{s}i_{s})^{2} + (C_{\alpha}\tan\alpha)^{2}}}\right] \\ F_{x} &= F_{xa} + F_{xs} = \frac{\mu WC_{s}i_{s}}{\sqrt{(C_{s}i_{s})^{2} + (C_{\alpha}\tan\alpha)^{2}}} \left[1 - \frac{\mu W(1-i_{s})}{4\sqrt{(C_{s}i_{s})^{2} + (C_{\alpha}\tan\alpha)^{2}}}\right] \\ f_{yaa} &= \int_{0}^{l_{c}} [k'_{y}x \tan\alpha/(1-i_{s})] \, dx = \frac{\mu^{2}W^{2}C_{\alpha}\tan\alpha(1-i_{s})}{4[(C_{s}i_{s})^{2} + (C_{\alpha}\tan\alpha)^{2}]} \\ F_{y\alpha} &= F_{y\alpha a} + F_{y\alpha s} = \frac{\mu WC_{\alpha}\tan\alpha}{\sqrt{(C_{s}i_{s})^{2} + (C_{\alpha}\tan\alpha)^{2}}} \left[1 - \frac{\mu W(1-i_{s})}{2\sqrt{(C_{s}i_{s})^{2} + (C_{\alpha}\tan\alpha)^{2}}}\right] \\ F_{y\alpha} &= F_{y\alpha a} + F_{y\alpha s} = \frac{\mu WC_{\alpha}\tan\alpha}{\sqrt{(C_{s}i_{s})^{2} + (C_{\alpha}\tan\alpha)^{2}}} \left[1 - \frac{\mu W(1-i_{s})}{4\sqrt{(C_{s}i_{s})^{2} + (C_{\alpha}\tan\alpha)^{2}}}\right] \\ F_{yca} &= F_{y\alpha a} + F_{y\alpha s} = \frac{\mu WC_{\alpha}\tan\alpha}{\sqrt{(C_{s}i_{s})^{2} + (C_{\alpha}\tan\alpha)^{2}}} \left[1 - \frac{\mu W(1-i_{s})}{4\sqrt{(C_{s}i_{s})^{2} + (C_{\alpha}\tan\alpha)^{2}}}\right] \\ F_{yca} &= F_{y\alpha a} + F_{y\alpha s} = \frac{\mu WC_{\alpha}\tan\alpha}{\sqrt{(C_{s}i_{s})^{2} + (C_{\alpha}\tan\alpha)^{2}}} \left[1 - \frac{\mu W(1-i_{s})}{4\sqrt{(C_{s}i_{s})^{2} + (C_{\alpha}\tan\alpha)^{2}}}\right] \\ F_{yca} &= F_{y\alpha a} + F_{y\alpha s} = \frac{\mu WC_{\alpha}\tan\alpha}{\sqrt{(C_{s}i_{s})^{2} + (C_{\alpha}\tan\alpha)^{2}}} \left[1 - \frac{\mu W(1-i_{s})}{4\sqrt{(C_{s}i_{s})^{2} + (C_{\alpha}\tan\alpha)^{2}}}\right] \\ F_{yca} &= F_{y\alpha a} + F_{y\alpha s} = \frac{\mu WC_{\alpha}\tan\alpha}{\sqrt{(C_{s}i_{s})^{2} + (C_{\alpha}\tan\alpha)^{2}}} \left[1 - \frac{\mu W(1-i_{s})}{4\sqrt{(C_{s}i_{s})^{2} + (C_{\alpha}\tan\alpha)^{2}}}\right] \\ F_{yca} &= F_{y\alpha a} + F_{y\alpha s} = \frac{\mu WC_{\alpha}\tan\alpha}{\sqrt{(C_{s}i_{s})^{2} + (C_{\alpha}\tan\alpha)^{2}}} \left[1 - \frac{\mu W(1-i_{s})}{4\sqrt{(C_{s}i_{s})^{2} + (C_{\alpha}\tan\alpha)^{2}}}\right] \\ F_{yca} &= F_{y\alpha a} + F_{y\alpha s} = \frac{\mu WC_{\alpha}\tan\alpha}{\sqrt{(C_{s}i_{s})^{2} + (C_{\alpha}\tan\alpha)^{2}}} \left[1 - \frac{\mu W(1-i_{s})}{4\sqrt{(C_{s}i_{s})^{2} + (C_{\alpha}\tan\alpha)^{2}}}\right]$$

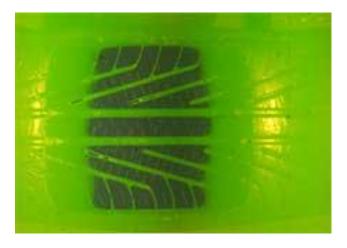
## Magic Formula

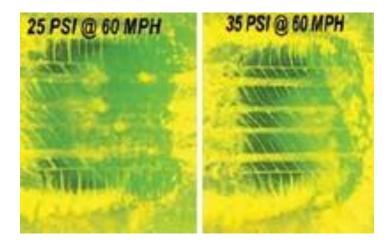


# Hydroplaning



# Hydroplaning





25 PSI @ 60 MPH



30 PSI @ 60 MPH



95-07-13