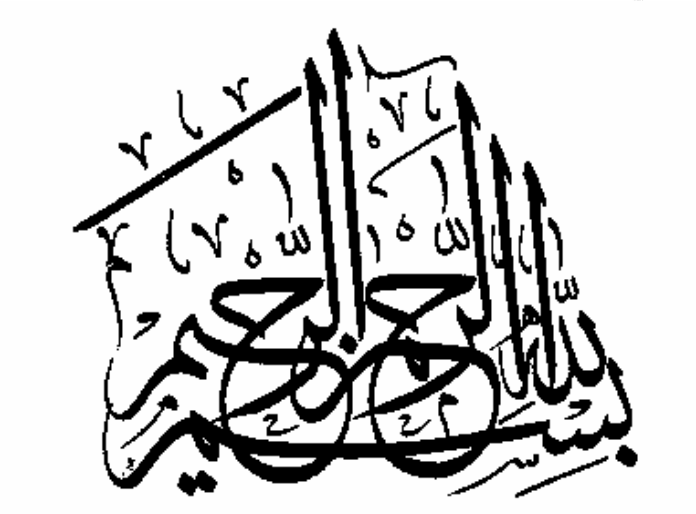
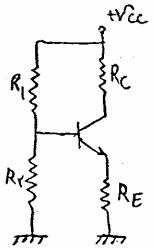
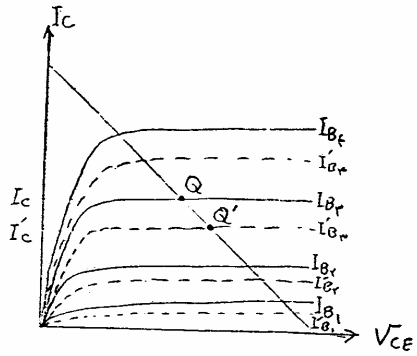


"" جزوه الکترونیک 1 – بخش دوم ""

تهیه کننده : حامد مظاهری
Hamed.Mazaher@Gmail.com



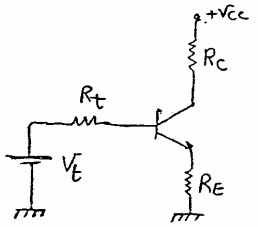


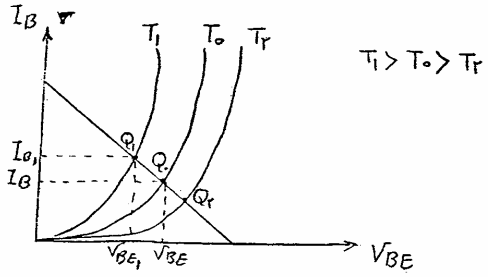
پایداری نقطهٔ کار

* I_{CBO}
* V_{BE}
* β
V_{CC}
R

به ازای تغییرات β بین β_{min} و β_{max}، جریانهای I_{Bi} به I'_{Bi} تبدیل می‌شوند.

$$V_{CC} \cong (R_C + R_E) I_C + V_{CE} \quad , \quad I_C = \beta I_B + I_{CEO}$$





$T_1 > T_0 > T_2$

$$V_t = R_t I_B + V_{BE} + R_E (1+\beta) I_B$$

$$I_C \rightarrow f(I_{CBO}, V_{BE}, \beta, \ldots)$$

ضرایب پایداری حرارتی

برای نمایش تغییرات I_C از dI_C یا $\Delta I_C = I_{C_1} - I_{C_0}$ استفاده می‌کنیم که اگر تغییرات I_C نسبت به پارامترهای f به صورت خطی باشد آن گاه، $dI_C = \Delta I_C$

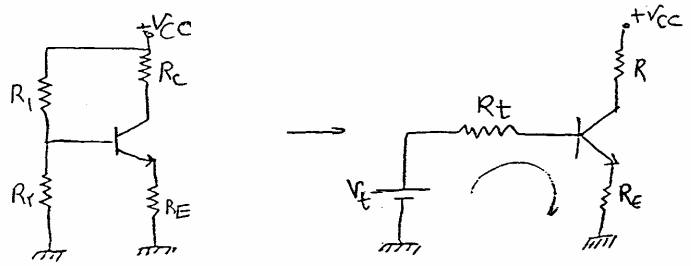
$$dI_C = \frac{\partial I_C}{\partial I_{CBO}} dI_{CBO} + \frac{\partial I_C}{\partial I_B} d\beta + \frac{\partial I_C}{\partial V_{BE}} dV_{BE}$$

ضرایب تغییرات وسیع : $S_{I_{CBO}} = S_I = \frac{\Delta I_C}{\Delta I_{CBO}}$, $S_{V_{BE}} = S_V = \frac{\Delta I_C}{\Delta V_{BE}}$

$$, \quad S_B = \frac{\Delta I_C}{\Delta B}$$

در تغییرات کم $\quad S_I \simeq \frac{\partial I_C}{\partial I_{CBO}} \quad , \quad S_V \simeq \frac{\partial I_C}{\partial V_{BE}}$

$$, \quad S_\beta \simeq \frac{\partial I_C}{\partial \beta}$$



$$\begin{cases} I_C = \beta I_B + (1+\beta) I_{CBO} \\ V_t = R_t I_B + V_{BE} + R_E (1+\beta) I_B \end{cases}$$

$$\longrightarrow \quad I_C = \frac{\beta}{R_E(1+\beta) + R_t} (V_t - V_{BE}) + \frac{(1+\beta)(R_E + R_t)}{R_E(1+\beta) + R_t} I_{CBO}$$

$$\longrightarrow \quad S_I = \frac{\partial I_C}{\partial I_{CBO}} = (1+\beta) \times \frac{1 + R_t/R_E}{(1+\beta) + R_t/R_E}$$

if $\quad R_t \ll R_E \quad \longrightarrow \quad S_I = 1$

if $\quad R_t \ll (1+\beta) R_E \quad \longrightarrow \quad R_t = \frac{(1+\beta) R_E}{10}$

$$\longrightarrow \quad S_I = 1 + \frac{R_t}{R_E}$$

$$S_V = \frac{\partial I_C}{\partial V_{BE}} = -\frac{\beta}{R_E(1+\beta) + R_t}$$

if $\quad R_t \ll (1+\beta) R_E \quad \longrightarrow \quad S_V = -\frac{1}{R_E}$

برای محاسبهٔ S_β :

$$V_t - V_{BE} \gg (R_E + R_t) I_{CBO} \longrightarrow I_C \simeq \frac{\beta}{R_E(1+\beta)+R_t}(V_t - V_{BE})$$

$$T_1 \longrightarrow I_{C_1}, \beta_1 \longrightarrow I_{C_1} = \frac{\beta_1}{R_E(1+\beta_1)+R_t}(V_t - V_{BE})$$

$$T_2 \longrightarrow I_{C_2}, \beta_2 \longrightarrow I_{C_2} = \frac{\beta_2}{R_E(1+\beta_2)+R_t}(V_t - V_{BE})$$

$$\Delta I_C = I_{C_2} - I_{C_1}, \quad \Delta\beta = \beta_2 - \beta_1, \quad \frac{I_{C_1}}{I_{C_2}} = \frac{\beta_1}{\beta_2} \times \frac{R_E(1+\beta_2)+R_t}{R_E(1+\beta_1)+R_t}$$

$$\longrightarrow \frac{I_{C_2} - I_{C_1}}{I_{C_2}} = \frac{\Delta I_C}{I_{C_1}} = \frac{\Delta\beta(R_t+R_E)}{\beta_1(R_t+(1+\beta_2)R_E)}$$

$$\longrightarrow S_\beta = \frac{\Delta I_C}{\Delta\beta} = \frac{I_{C_1}(R_t+R_E)}{\beta_1[R_t+(1+\beta_2)R_E]}$$

$$\Delta I_C = \left(1+\frac{R_t}{R_E}\right)\Delta I_{CBO} - \frac{1}{R_E}\Delta V_{BE} + \frac{I_{C_1}}{\beta_1}\cdot\frac{R_E+R_t}{R_t+(1+\beta)R_2}\Delta\beta +$$

رابطهٔ بالا وقتی است که $R_t \ll (1+\beta)R_E$

$$\Delta I_C = S_I \Delta I_{CBO} + S_V \Delta V_{BE} + S_\beta \Delta\beta + S_{V_{CC}} \Delta V_{CC} + S_R \Delta R +$$

مثال :

$R_C = 4\,k\Omega$, $V_{CC} = 20\,V$, $\begin{cases} I_C = 2\,mA \\ V_{CE} = 10\,V \end{cases}$

$24 < \beta < 90$, $1.75\,mA < I_C < 2.25\,mA$, R_1, R_2

$$\longrightarrow V_{CC} = (R_E + R_C) I_C + V_{CE} \longrightarrow R_E = 1\,k\Omega$$

$$S_\beta = \frac{\Delta I_C}{\Delta\beta} = \frac{I_{C_2} - I_{C_1}}{\beta_2 - \beta_1} = \frac{2.25 - 1.75}{90 - 24} = \frac{I_{C_1}(R_t+R_E)}{\beta_1[R_t+(1+\beta_2)R_E]}$$

$\longrightarrow R_t = 20.1\ k\Omega$

$$\begin{cases} R_1 = \dfrac{V_t}{V_{CC}} R_t \\ R_2 = \dfrac{R_t}{1 - \frac{V_{CC}}{V_t}} \end{cases}$$

$$V_t = R_t I_\beta + V_{BE} + R_E I_E \quad (I_\beta = I_C/\beta \ ,\ I_E = \tfrac{\beta+1}{\beta} I_C)$$

$$\longrightarrow 1.15\,mA < I_C \simeq I_E = \frac{V_t - V_{BE}}{\frac{R_t}{\beta} + R_E} < 2.12\,mA$$

$$\longrightarrow 1.15\left(\frac{R_t}{\beta_{min}} + R_E\right) < V_t - V_{BE} < 2.12\left(\frac{R_t}{\beta_{max}} + R_E\right)$$

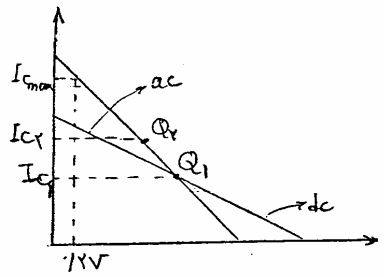
$$\longrightarrow 3.38 < V_t < 3.4 \longrightarrow \frac{R_1}{R_2}$$

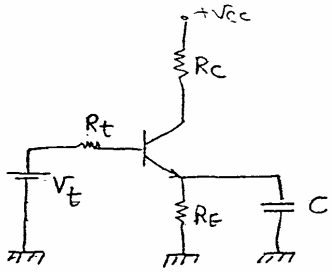
مثال: اگر $40 < \beta < 120$ ، $0.7V < V_{BE} < 0.8V$ باشد R_t, R_E, V_t را طوری پیدا کنید که

$V_{CC} = 15V$ ، $R_C = 1k\Omega$

$V_{CE_{sat}} = 1.2V$

سوئینگ $5\,mA$ در I_C را داشته باشیم.





$\longrightarrow I_{C_1} = 5\,mA$

(ac) تقریب $\quad v_{ce} = -R_C i_c$ $\quad$ ac خط بار

$\longrightarrow (V_{CE} - V_{CE}) = -R_C(i_C - I_C)$ ①

V_{CE} کلی $\quad V_{CE}$ dc

① ، ② $\longrightarrow I_{C_2} = \frac{9.8}{1+R_E}$

$V_{CC} \simeq R_C I_C + V_{CE} + R_E I_C$ dc خط بار ②

$$\longrightarrow \underbrace{5\,mA}_{I_{C_1}} < I_{CQ} < \underbrace{\frac{9.8}{1+R_E}}_{I_{C_2}}$$

$V_{CE} = 1.2V$ ، $I_{C_m} = I_{C_2} + 5\,mA$

$$\Delta I_C = I_{C_2} - I_{C_1} = \frac{9.8}{1+R_E} - 5 \longrightarrow \boxed{\Delta I_C = \frac{4.8 - 5R_E}{1+R_E}}$$

I

$$\Delta I_C = S_\beta \Delta\beta + S_V \cdot \Delta V_{BE}$$

$$\frac{\Delta I_C}{I_C} = \frac{I_C}{\beta_1} \times \frac{R_t + R_E}{R_t + (1+\beta_1)R_E}\Delta\beta - \frac{1}{R_E}\Delta V_{BE} \longrightarrow \boxed{\Delta I_C = \frac{1}{R_E} + \frac{1}{\Delta}} \quad \text{II}$$

$$R_t \ll (1+\beta)R_E \xrightarrow{\text{انتخاب}} R_t = \frac{\beta_{min} \cdot R_E}{10}$$

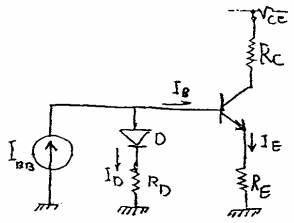
$$I, II \longrightarrow R_E = 44\,\Omega, \ \boxed{R_E = 720\,\Omega}$$

$$\longrightarrow R_t = 1.9\,k\Omega, \quad I_{C1} = 5\,mA, \quad I_{C2} = 5.48\,mA$$

$$\longrightarrow 5 < I_C < 5.48$$

$$\longrightarrow 5 < \frac{V_t - V_{BE}}{R_E + \frac{R_t}{\beta}} < 5.48 \xrightarrow{\text{جزئیات حل کنید}} 4.1 < V_t < 4.4$$

$$\longrightarrow \boxed{\begin{array}{l} V_t = 4.2\,V \\ R_b = 1.1\,k\Omega \\ R_e = 750\,\Omega \end{array}}$$



جبران اثر حرارتی:

V_{BE}

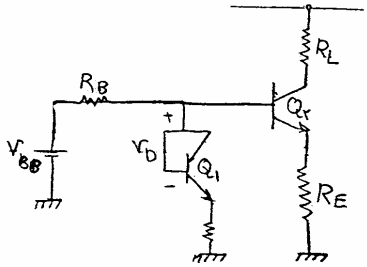
I_{CBO}

β

$$\begin{cases} I_{BB} = I_D + I_B \\ V_D + R_D I_D = V_{BE} + R_E I_E \end{cases}$$

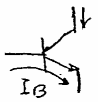
$$\longrightarrow I_E = \frac{V_D - V_{BE} + I_{BB}R_D}{R_E + \frac{R_D}{1+\beta}}$$

$$\longrightarrow \frac{\Delta I_E}{\Delta T} = \frac{\frac{\Delta V_D}{\Delta T} - \frac{\Delta V_{BE}}{\Delta T}}{R_E + R_D/1+\beta} \longrightarrow \frac{\Delta V_D}{\Delta T} = \frac{\Delta V_{BE}}{\Delta T} = -K$$

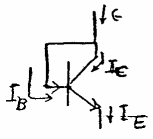


استفاده از ترانزیستور Q_1 به جای دیود مطرح است.

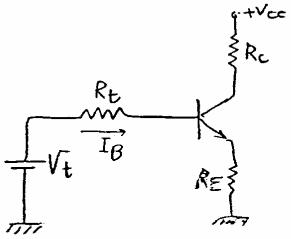
این مزیت را دارد که اختلاف ورودی ترانزیستور کم است.



$$h_{ie} = \frac{\eta V_T}{I_C}$$



$$\frac{h_{ie}}{1+h_{fe}}$$



$$R_t = R_D \parallel R_B$$

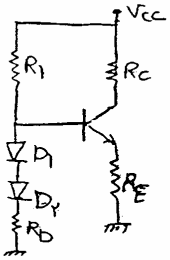
$$V_t = \frac{R_D V_{BB} + R_B V_D}{R_D + R_B}$$

$$V_t = R_t I_B + V_{BE} + R_E I_E$$

$$\rightarrow I_E = \frac{(V_{BB} R_D + V_D R_B)/(R_B + R_D)}{R_E}$$

$$\rightarrow \frac{\Delta I_E}{\Delta T} = \frac{1}{R_E}\left[\frac{\Delta V_D}{\Delta T}\cdot\frac{R_B}{R_B+R_D} - \frac{\Delta V_{BE}}{\Delta T}\right]$$

$$, \quad \frac{\Delta V_D}{\Delta T} = \frac{\Delta V_{BE}}{\Delta T} = -K \qquad \rightarrow \frac{\Delta I_E}{\Delta T} = \frac{K}{R_E}\left[\frac{1}{1+\frac{R_B}{R_D}}\right]$$

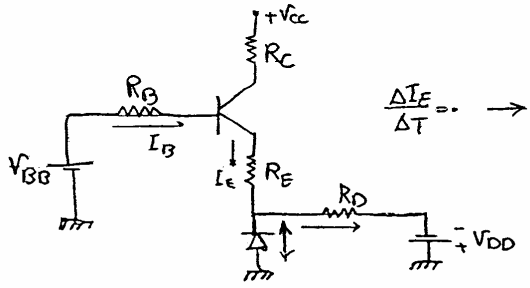


$$V_t = \frac{V_{CC} R_D + 2V_D R_B}{R_D + R_B}$$

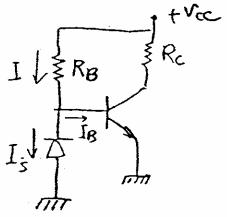
$$R_t = R_D \parallel R_B$$

$$I_E = \frac{(V_{CC} R_D + 2V_D R_B)/(R_B + R_D) - V_{BE}}{R_E}$$

$$\frac{\Delta V_D}{\Delta T} = \frac{\Delta V_{BE}}{\Delta T} \rightarrow \frac{\Delta I_E}{\Delta T} = 0 \rightarrow R_B = R_D$$



$\frac{\Delta I_E}{\Delta T} = 0 \rightarrow \frac{\Delta V_{BE}}{\Delta T} = \frac{\Delta V_D}{\Delta T}$ شرط اینکه : تمرین : با

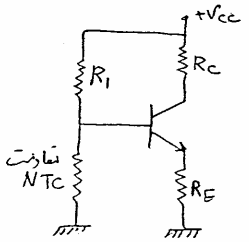


جبران اثر حرارتی I_{CBO} :

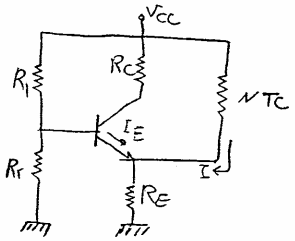
$$\begin{cases} I_C = \beta I_B + (1+\beta) I_{CBO} \\ I_C = \beta (I - I_S) + (1+\beta) I_{CBO} \end{cases}$$

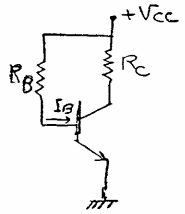
با فرض رفتار معادل یک دیود و ترانزیستور و β بزرگ

$$\longrightarrow \frac{\Delta I_C}{\Delta T} = -\beta \frac{\Delta I_S}{\Delta T} + (1+\beta) \frac{\Delta I_{CBO}}{\Delta T} \simeq 0 \qquad , \quad \beta \gg$$



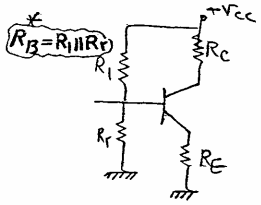
تثبیت کنندگی حرارتی با استفاده از مقاومت‌های PTC , NTC :





$$\Delta I_C = S_I \frac{\Delta I_C}{\Delta I_{CBO}} + \cdots$$

$$S_0 = \frac{\Delta I_C \text{ مدار بدون پایداری}}{\Delta I_C \text{ مدار پایدار}}$$



I_{CEO}

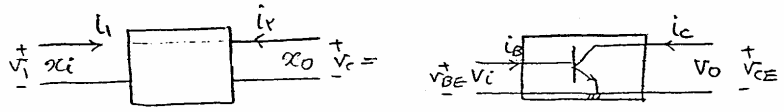
$$\frac{\Delta I_C}{\Delta I_{CEO}} \simeq 1 \longrightarrow I_C = \beta I_B + (1+\beta) I_{CBO}$$

$$\longrightarrow S_0 = \frac{1}{\left(\frac{R_B^* + R_E(1+\beta)}{R_B^* + R_E}\right)^{-1}} = \frac{R_B(1+\beta)}{R_B^* + R_E} \longrightarrow R_B^* \ll (1+\beta) R_E$$

$$\longrightarrow S_0 = \frac{(1+\beta) R_E}{R_B^* + R_E}$$

$$S_0 = 1 + \frac{\beta R_E}{R_E + R_B} \qquad , \quad \beta \gg$$

$$S_0 > 1$$



$$\text{Z امپدانس}\begin{cases} V_1 = Z_{11} i_1 + Z_{12} i_2 \\ V_2 = Z_{21} i_1 + Z_{22} i_2 \end{cases}$$

$$\text{هیبرید } h\begin{cases} V_1 = h_{11} i_1 + h_{12} V_2 \\ i_2 = h_{21} i_1 + h_{22} V_2 \end{cases}$$

$$\text{ادمیتانس } Y\begin{cases} i_1 = y_{11} V_1 + y_{12} V_2 \\ i_2 = y_{21} V_1 + y_{22} V_2 \end{cases}$$

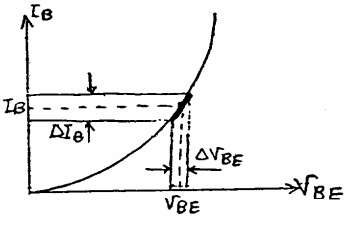
$$\begin{cases} Z_{11} = \dfrac{V_1}{i_1}\Big|_{i_2=0} & \text{امپدانس ورودی خروجی باز} \\ Z_{22} = \dfrac{V_2}{i_2}\Big|_{i_1=0} & \text{امپدانس خروجی ورودی باز} \\ Z_{12} = \dfrac{V_1}{i_2}\Big|_{i_1=0} & \text{امپدانس انتقالی معکوس} \\ Z_{21} = \dfrac{V_2}{i_1}\Big|_{i_2=0} & \text{امپدانس انتقالی مستقیم} \end{cases}$$

$$\begin{cases} y_{11} = \dfrac{i_1}{V_1}\Big|_{V_2=0} & \text{ادمیتانس ورودی} \\ y_{22} = \dfrac{i_2}{V_2}\Big|_{V_1=0} & \text{ادمیتانس خروجی} \\ y_{12} = \dfrac{i_1}{V_2}\Big|_{V_1=0} & \text{ادمیتانس انتقالی معکوس} \\ y_{21} = \dfrac{i_2}{V_1}\Big|_{V_2=0} & \text{ادمیتانس انتقالی مستقیم} \end{cases}$$

$$\begin{cases} h_{11} = \dfrac{V_1}{i_1}\Big|_{V_2=0} & \text{امپدانس ورودی } (h_{ie}) \\ h_{22} = \dfrac{i_2}{V_2}\Big|_{i_1=0} & \text{ادمیتانس خروجی } (h_{oe}) \\ h_{12} = \dfrac{V_1}{V_2}\Big|_{i_1=0} & \text{بهره ولتاژ انتقالی معکوس } (h_{re}) \\ h_{21} = \dfrac{i_2}{i_1}\Big|_{V_2=0} & \text{بهره جریان انتقالی مستقیم } (h_{fe}) \end{cases}$$

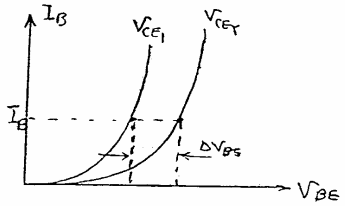
امپدانس ترانزیستور

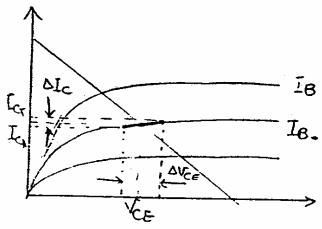
$$h_{11} = h_{ie} = \frac{\Delta V_{BE}}{\Delta I_B}\Big|_{V_{CE}\ \text{ثابت}}$$



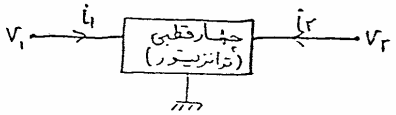
59

$$h_{12} = h_{re} = \left.\frac{\Delta V_{BE}}{\Delta V_{CE}}\right|_{I_B} \text{ ثابت}$$





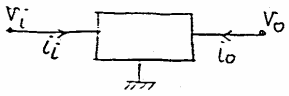
مدار هیبرید :



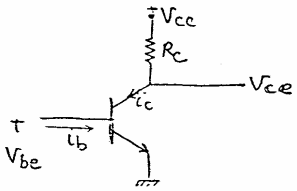
پارامترهای h

$$\begin{cases} V_1 = h_{11} i_1 + h_{12} V_2 \\ i_2 = h_{21} i_1 + h_{22} V_2 \end{cases}$$

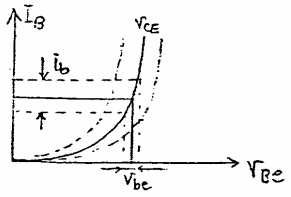
$$\begin{cases} V_i = h_{ie} i_i + h_{re} V_o \\ i_o = h_{fe} i_i + h_{oe} V_o \end{cases}$$

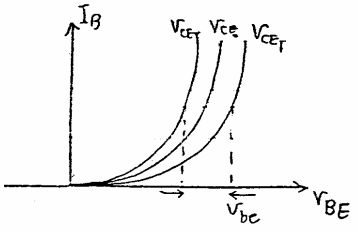


$$\begin{cases} V_{be} = h_{ie} i_b + h_{re} V_{ce} \\ i_c = h_{fe} i_b + h_{oe} V_{ce} \end{cases}$$

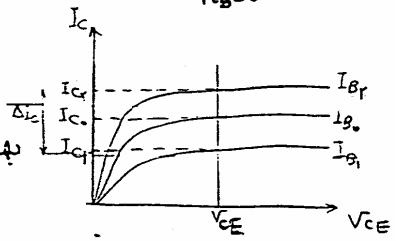


$h_{ie} = \left.\frac{V_{be}}{i_b}\right|_{V_{ce}=0}$ امپدانس ورودی



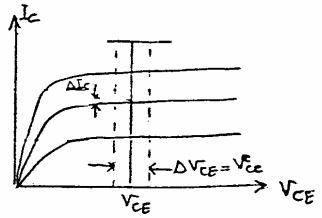


$h_{re} = \left.\frac{V_{be}}{V_{ce}}\right|_{i_b=0}$ بهره ولتاژ معکوس

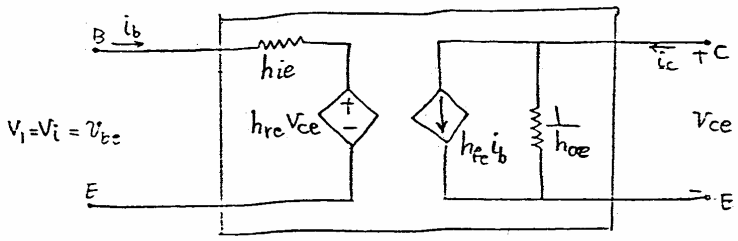


$h_{fe} = \left.\frac{i_c}{i_b}\right|_{V_{ce}=0}$ بهره جریان مستقیم

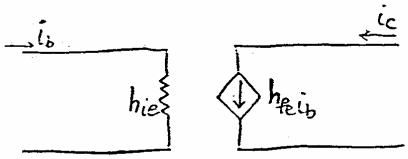
$$\begin{cases} i_b - \Delta I_B = I_{B_2} - I_{B_1} \\ i_c = \Delta I_C = I_{C_2} - I_{C_1} \end{cases}$$



$h_{oe} = \left.\frac{i_c}{V_{ce}}\right|_{i_b=0}$ ادمیتانس خروجی

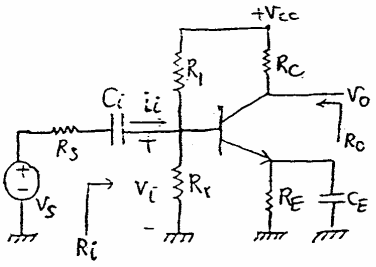


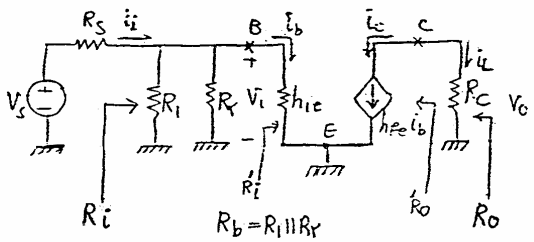
مدل هیبرید C.E (دقیق)



مدل تقریبی

مدار معادل ac :





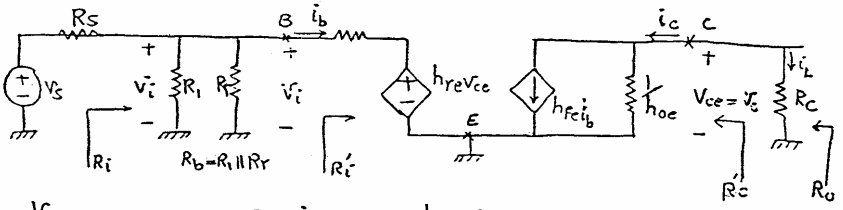
گین ولتاژ $A_V = \frac{V_o}{V_i}$ گین جریان $A_i = \frac{i_L}{i_i}$

$$A_V = \frac{V_o}{V_i} = \frac{-R_C i_c}{h_{ie} i_b} A_i' \longrightarrow A_V = -\frac{h_{fe} \cdot R_o}{h_{ie}} = -\frac{R_o}{R_i'} A_i'$$

$$A_i = \frac{i_L}{i_i} = \frac{-i_c}{i_b} \times \frac{i_b}{i_i} = h_{fe} \times \frac{R_b}{R_b + h_{ie}} \longrightarrow A_i = h_{fe} \frac{R_b}{R_b + h_{ie}}$$

$$R_i = \frac{V_i}{i_i} = R_1 \| R_Y \| R_i' = R_1 \| R_Y \| \left(\frac{V_i}{i_b}\right) = R_1 \| R_Y \| h_{ie} \longrightarrow R_i = R_1 \| R_Y \| h_{ie}$$

$$R_o = \left.\frac{V_o}{i_o}\right|_{V_S = 0} = R_o' \| R_C = \infty \| R_C = R_C \longrightarrow R_o = R_C$$



$$A_V = \frac{V_o}{V_i} \rightarrow \begin{cases} V_o = -R_C \cdot i_C = -R_C (h_{fe} i_b + V_o h_{oe}) \\ V_i = h_{ie} i_b + h_{re} V_{ce} = h_{ie} i_b + h_{re} V_o \end{cases}$$

$$\rightarrow A_V = \frac{-h_{fe} (R_C \| \frac{1}{h_{oe}})}{h_{ie} - h_{re} h_{fe} (R_C \| \frac{1}{h_{oe}})}$$

$$R_i = \frac{V_i}{i_i} = R_1 \| R_2 \| R'_i = R_1 \| R_2 \| \frac{V_i}{i_b} = R_1 \| R_2 \| R'_i$$

$$, R'_i = h_{ie} - h_{re} h_{fe} (R_C \| \frac{1}{h_{oe}})$$

$$\rightarrow R_i = R_1 \| R_2 \| \left(h_{ie} - h_{re} h_{fe} (R_C \| \frac{1}{h_{oe}}) \right)$$

$$A_i = \frac{i_C}{i_b} = \quad , \quad A_V = \frac{R_o}{R'_i} \times A_i$$

$$, A_i = \frac{i_C}{i_b} = \frac{i_C}{h_{fe} i_b} \times \frac{h_{fe} i_b}{i_b} = \frac{\frac{1}{h_{oe}}}{\frac{1}{h_{oe}} + R_C} \times h_{fe} \rightarrow A_i = \frac{\frac{1}{h_{oe}}}{\frac{1}{h_{oe}} + R_C} \cdot h_{fe}$$

$$A_{i_S} \triangleq \frac{i_C}{i_i} = \frac{i_C}{i_b} \times \frac{i_b}{i_i} = A_i \times \frac{R_b}{R_b + R'_i} \rightarrow A_{i_S} = A_i \frac{R_b}{R_b + R'_i}$$

$$R_o = \left. \frac{V_o}{i_o} \right|_{V_S = 0} = R_C \| R'_o$$

$$R'_o = \left. \frac{V_o}{i_C} \right|_{V_S = 0} = \quad , \quad i_C = h_{fe} i_b + V_o h_{oe} \quad (i_b =) \quad , \quad h_{re} V_o = i_b (h_{ie} + R_S \| R_b)$$

$$\rightarrow Y_o = \frac{1}{R'_o} = h_{oe} - \frac{h_{fe} h_{re}}{h_{ie} + R_S \| R_b}$$

مثال عددی: $R_C = 1k\Omega$ ، $R_S = 100\Omega$ ، $R_b \gg h_{ie}$

$h_{fe} = \beta = 50$ ، $h_{ie} = 1100\Omega$ ، $h_{re} = 2.5 \times 10^{-4}$ $h_{oe} = 25\mu s$

$\rightarrow \frac{1}{h_{oe}} = 40k\Omega$

الف) مقدار A_V، R_i، R_o'، A_i را با فرض h_{oe} و h_{re} به طور دقیق بدست آورید. ب) با فرض $R_o = R_C \| R_o'$ را به طور تقریباً صفر مقادیر قسمت الف را بدست آورید.

الف)

$$\longrightarrow A_V = \frac{-h_{fe}(R_C \| \frac{1}{h_{oe}})}{h_{ie} - h_{re} h_{fe} R_C} = -44$$

$$R_i = R_i' = h_{ie} - h_{re} h_{fe} R_L = 1.09K \simeq 1.1K\Omega$$

$$A_i = -50.4 = \frac{-i_C}{i_b} \overset{\text{طبق تقسیم جریان}}{=} \frac{-i_C}{i_i}$$

$$Y_o = h_{oe} - \frac{h_{fe} h_{re}}{h_{ie} + R_S \| R_b} = 1.14 \times 10^{-4} S \longrightarrow R_o' = \frac{1}{Y_o} \simeq 25K$$

$$R_o = R_C \| R_o' \simeq 1k\Omega$$

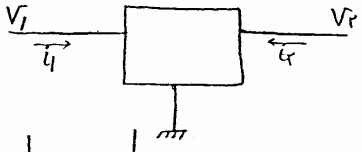
ب)

$$\longrightarrow R_i = R_b \| h_{ie} = 1.1k\Omega$$

$$R_o = R_o' \| R_C = \infty \| R_C = R_C = 1k\Omega$$

$$A_V = \frac{-h_{fe} R_C}{h_{ie}} = -45.5$$

$$A_i = \frac{-i_C}{i_b} = -h_{fe} = -50$$



$$\begin{cases} V_1 = h_{11} i_1 + h_{12} V_2 \\ i_2 = h_{21} i_1 + h_{22} V_2 \end{cases} \qquad \begin{matrix} \text{Common Collector} \\ C.C \end{matrix} \rightarrow \begin{cases} V_{bc} = h_{ic} i_b + h_{rc} V_{ec} \\ i_e = h_{fc} i_b + h_{oc} V_{ec} \end{cases}$$

h_i , h_r , h_f , h_o

$$h_{ic} = \left.\frac{V_{bc}}{i_b}\right|_{V_{ec}=0}$$ امپدانس ورودی

$$h_{rc} = \left.\frac{V_{bc}}{V_{ec}}\right|_{i_b=0}$$ بهرهٔ ولتاژ انتقالی معکوس

$$h_{fc} = \left.\frac{i_e}{i_b}\right|_{V_{ec}=0}$$ بهرهٔ جریان مستقیم

$$h_{oc} = \left.\frac{i_e}{V_{ec}}\right|_{i_b=0}$$ ادمیتانس خروجی

$$V_{bc} = V_{be} + V_{ec} = V_{be} = h_{ie} \times i_b$$

$$\rightarrow h_{ic} = \left.\frac{V_{bc}}{i_b}\right|_{V_{ec}=0} = \frac{h_{ie} \times i_b}{i_b} = h_{ie} \rightarrow \boxed{h_{ic} = h_{ie}}$$

$$h_{rc} = \left.\frac{V_{be} + V_{ec}}{V_{ec}}\right|_{i_b=0} = \frac{h_{re} \cdot V_{ec} + V_{ec}}{V_{ec}} = 1 - h_{re}$$

$$V_{be} = h_{ie} i_b + h_{re} V_{ce} = -h_{re} V_{ec} \quad (i_b = 0)$$

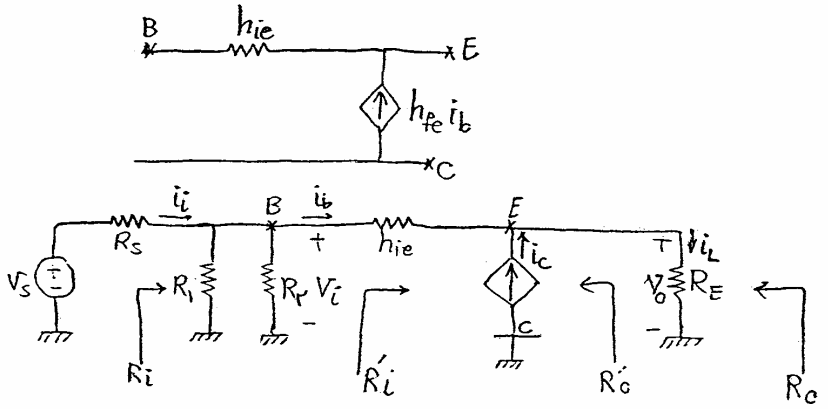
$$\rightarrow \boxed{h_{rc} = 1 - h_{re}}$$

$$h_{fc} = \left.\frac{i_e}{i_b}\right|_{V_{ec}=0} \rightarrow h_{fc} = \left.\frac{-(1+h_{fe}) i_b}{i_b}\right|_{V_{ec}=0} = -(1+h_{fe})$$

$V_{ec} = 0 \rightarrow i_c = h_{fe} i_b$

$$\rightarrow \boxed{h_{fc} = -(1+h_{fe})}$$

$$h_{oc} = \left.\frac{i_e}{V_{ec}}\right|_{i_b=0} = \frac{-i_c}{i_c \times \frac{1}{h_{oe}}} = h_{oe} \longrightarrow \boxed{h_{oc} = h_{oe}}$$



$$A_i = \frac{i_L}{i_i} = \frac{i_L}{i_b} \cdot \frac{i_b}{i_i} = \frac{i_b + h_{fe} i_b}{i_b} \cdot \frac{R_b}{R_b + R'_i}$$

$$A_V = \frac{V_o}{V_i} = \frac{(1+h_{fe})\, i_b \cdot R_E}{(1+h_{fe}) i_b \cdot R_E + h_{ie} \cdot i_b} = \frac{(1+h_{fe}) R_E}{h_{ie} + (1+h_{fe}) R_E} \simeq 1$$

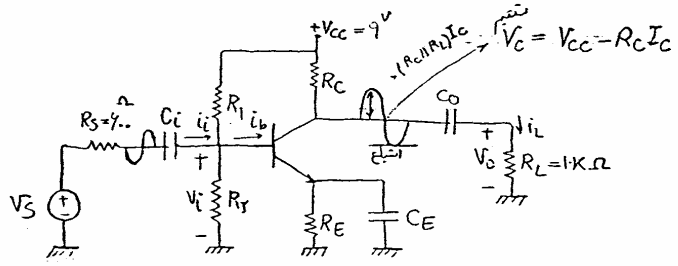
$$\longrightarrow A_V = \frac{(1+h_{fe})\, R_E}{h_{ie} + (1+h_{fe})\, R_E}$$

$$R_i = \frac{V_i}{i_i} = R_1 \| R_2 \| R'_i$$

$$R'_i = \frac{V_i}{i_b} = \frac{(1+h_{fe}) i_b \cdot R_E + h_{ie} \cdot i_b}{i_b} = (1+h_{fe}) R_E + h_{ie}$$

$$R_o = \left.\frac{V_o}{i_o}\right|_{V_s=0} = R'_o \| R_E$$

$$R'_o = \left.\frac{V_o}{i_e}\right|_{V_s=0} = \frac{-i_b \cdot h_{ie} - i_b \cdot R_1 \| R_2 \| R_s}{-(1+h_{fe})\, i_b} = \frac{h_{ie} + R_1 \| R_2 \| R_s}{(1+h_{fe})}$$



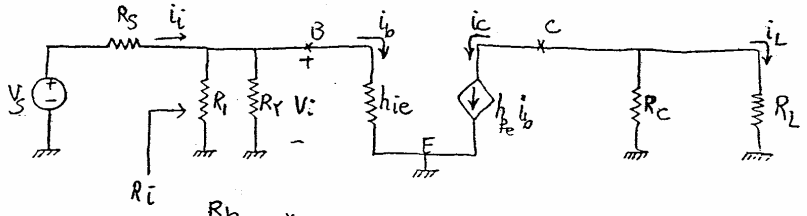
مدار مقابل را با داده های

زیر طراحی کنید.

$V_C = V_{CC} - R_C I_C$ نقطه

داده ها :

$\beta = h_{fe} = 200$ ، $\frac{i_L}{i_i} = A_i \geq 120$ ، $R_i \geq 2\,K\Omega$ ، $V_{o_{PP}} \geq 2V$



برای راحتی کار از تقریب مقابل استفاده می کنیم : $\frac{R_b}{R_1 \| R_2} \overset{*}{\gg} h_{ie}$

$A_i \geq 120 \longrightarrow \frac{i_L}{i_i} = \frac{i_L}{i_b} = \frac{i_L}{i_C} \times \frac{i_C}{i_b} = \frac{-R_C}{R_C + R_L} \times h_{fe} \geq 120$

$\longrightarrow R_C \geq 1.0\,K\Omega$

مقاومتهای استاندارد
1.8 K
2.2 K
2.7 K
$R_C = \boxed{2.7\,K}$

$R_i \overset{*}{\simeq} h_{ie} \geq 2K\Omega$ ، $h_{ie} = \frac{\eta V_T \beta}{I_C} \geq 2K\Omega \longrightarrow \boxed{I_C \leq 3.5\,mA}$ ①

$(R_C \| R_L) I_C \geq 1V \longrightarrow \boxed{I_C \geq 1.37\,mA} \leftarrow V_{o_p}^{+}$ ②

چون $V_{CE_{sat}}$ را ندانسته آن را صفر می گیریم.

$V_{CC} = R_C I_C + V_{CE} + R_E I_C$

$\longrightarrow V_{CE} = V_{CC} - I_C(R_C + R_E) \geq 1\,V \longrightarrow I_C \leq \frac{8}{R_C + R_E}$

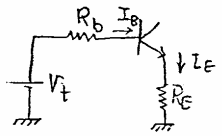
اگر $R_E = 0 \longrightarrow \boxed{I_C \leq 2.96\,mA} \leftarrow V_{o_p}$ ③

①، ②، ③ $\longrightarrow I_C = 2\,mA$

$$I_c \lesssim \frac{\Lambda}{R_E + R_C} \xrightarrow{I_C = ۲^{mA}} \boxed{R_E = ۱\,k\Omega}$$

$$R_b = \frac{\beta_{min} R_E}{۱۰} = ۲۰\,k\Omega$$

مدار DC:



$$\begin{cases} R_۱ = R_b \dfrac{V_{CC}}{V_t} \\ R_۲ = \dfrac{R_b}{1 - \frac{V_t}{V_{CC}}} \end{cases} \quad , \quad V_t = R_b I_B + V_{BE} + R_E I_E = ۲\,۱۹^{V}$$

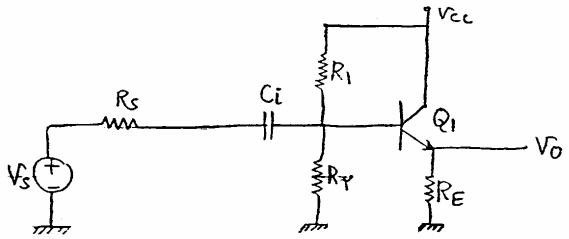
$$\longrightarrow \quad R_۱ = ۹۳\,k\Omega \quad , \quad R_۲ = ۲۸۱,۹\,K\Omega$$

$R_۱ = ۹۱\,k$ استاندارد — $R_۲ = ۲۲\,k$ استاندارد

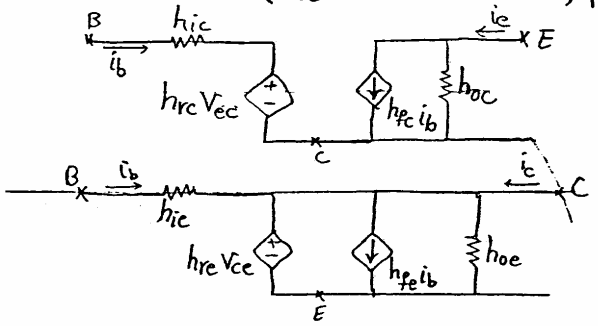
اگر اعداد بدست آمده را در مسئله قرار داده و یکبار دیگر تحلیل کنیم خواهیم دید که:

$$\longrightarrow \quad R_i = R_۱ \| R_۲ \| h_{ie} = ۲\,۱۹^{K\Omega} V \quad , \quad A_i = -۱۲۴ \quad , \quad V_{CE} = ۱,۹^{V}$$

تقویت کنندهٔ کلکتور مشترک:



با فرض اینکه پارامترهای هیبرید را در تقویت کنندهٔ امیتر مشترک داریم، پارامترهای هیبرید کلکتور مشترک را بدست می آوریم ($h_{oc}, h_{rc}, h_{fc}, h_{ic}$):



C.E.

مثال:

$R_E = R_L = 1\ K\Omega$, $R_s = 100\ \Omega$

$R_b = R_1 \| R_2 = 500\ K\Omega$, $h_{fe} = 50$, $h_{ie} = 1100\ \Omega$

مقادیر A_v ، R_i ، A_i ، R_o را بدست آورید:

$$A_V = \frac{(1+h_{fe})(R_E \| R_L)}{h_{ie} + (1+h_{fe})(R_E \| R_L)} = \frac{(51)(0.5)}{1.1 + 51(0.5)} = 0.98$$

$$R_i = R_b \| R'_i = R_b \| \left[h_{ie} + (1+h_{fe})(R_E \| R_L) \right] = 47\ K\Omega$$

$$A_i = \frac{i_L}{i_i} = \frac{i_L}{i_e} \cdot \frac{i_e}{i_b} \cdot \frac{i_b}{i_i} = \frac{R_E}{R_E + R_L} \cdot (1+h_{fe}) \cdot \frac{R_b}{R_b + R'_i} = 24\ K\Omega$$

می توان A_i را از رابطهٔ مقابل بدست آورد:

$$A_i = \frac{\overbrace{i_L R_L}^{V_o} R_i}{\underbrace{i_i \hat{R}_L \hat{R}_i}_{V_i}} = A_V \cdot \frac{R_i}{R_L}$$

$$R_O = R_E \| \frac{(R_S \| R_b) + h_{ie}}{1+h_{fe}} \simeq 23.5\ \Omega$$

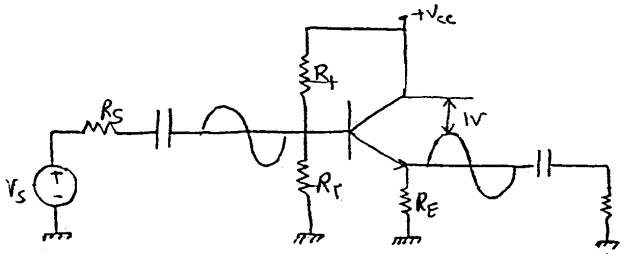
مثال: تقویت کنندهٔ کلکتور مشترکی با داده های زیر طراحی کنید:

$A_{VS} \geq 0.98$, $R_i \geq 15 K\Omega$, $V_{ip} = 2V \longrightarrow V_{op} = 2V$

$V_{CE_{min}} = 1^V$, $R_S = 100\ \Omega$, $R_L = 1\ K\Omega$, ترانزیستور BC107

$V_{CC} = 9^V$, $\beta = 1.4$, $V_T = 25^{mV}$

$150 < \beta < 200$

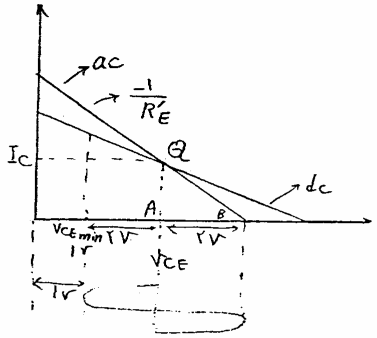


$$A_V = \frac{(1+h_{fe})(R_E \parallel R_L)}{h_{ie}+(1+h_{fe})(R_E \parallel R_L)} > 0.98 \longrightarrow \frac{h_{fe}(R_E \parallel R_L)}{\underbrace{\frac{\eta V_T \beta}{I_C}}_{h_{ie}} + h_{fe}(R_E \parallel R_L)} > 0.98$$

$$\longrightarrow 1+\frac{1}{R_E} < 0.085 I_C$$

$$V_{CC} = R_E I_C + V_{CE} \longrightarrow I_C = \frac{9 - V_{CE}}{R_E} \quad (*)$$

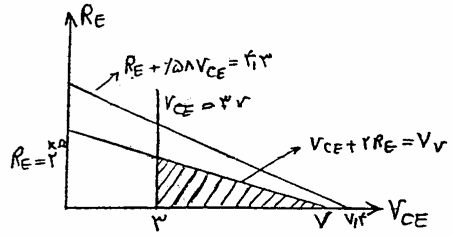
$$\longrightarrow R_E + 0.085 V_{CE} < 4.2 \quad (1)$$



$$\longrightarrow V_{CE} \geq 2\,V \quad (2) \qquad , \qquad AB = I_C \cdot R'_E > 2\,V \qquad , \qquad R'_E = \frac{R_E \cdot R_L}{R_E + R_L}$$

$$\longrightarrow I_C \cdot \frac{R_E}{1+R_E} > 2\,V$$

$$(*) \longrightarrow 2R_E + V_{CE} < V_T \quad (3)$$



$$\longrightarrow R_E = 1.5\,k\Omega \text{ (مقاومت استاندارد)} \longrightarrow V_{CE} = 4\,V \quad , \quad I_C = \frac{V_{CC}-V_{CE}}{R_E} = 3.3\,mA$$

$$R_i = R'_i \parallel R_b = \left[h_{ie} + (1+h_{fe})(R_E \parallel R_L)\right] \parallel R_b > 15\,k$$

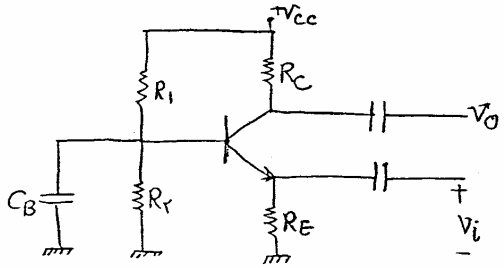
$$, \quad h_{ie_{min}} = \frac{\eta V_T \beta_{min}}{I_C} = 1.94\,k\Omega$$

$$\longrightarrow R_b > 18.1\,k\Omega$$

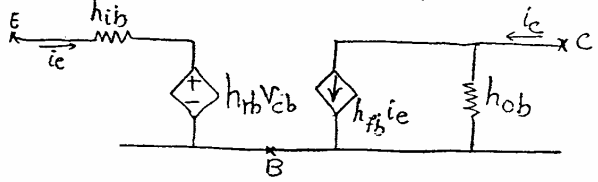
$$R_b = \frac{\beta_{min} \cdot R_E}{10} \simeq 18\ k\Omega \longrightarrow R_1 \| R_2 = 18\ k\Omega$$

با اندکی تغییر $\longrightarrow$ $R_1 = 30k$ (استاندارد) $\rightarrow 33k$ ، $R_2 = 50k$ (استاندارد) $\rightarrow 47k$

تقویت کنندهٔ بیس مشترک :



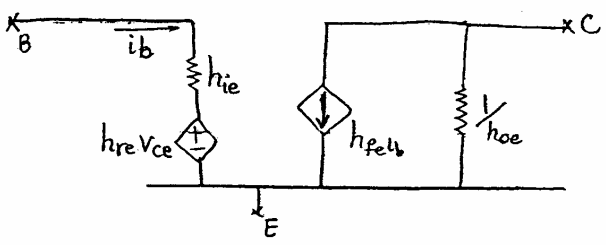
استفاده از خازن C_B صرفاً برای افزایش گین است.



$$\begin{cases} V_{eb} = h_{ib} \cdot ie + h_{rb} V_{cb} \\ ic = h_{fb}\, ie + V_{cb}\, h_{ob} \end{cases}$$

$$h_{ib} = \left.\frac{V_{eb}}{ie}\right|_{V_{cb}=0} \quad , \quad h_{rb} = \left.\frac{V_{eb}}{V_{cb}}\right|_{ie=0}$$

$$h_{fb} = \left.\frac{ic}{ie}\right|_{V_{cb}=0} \qquad h_{ob} = \left.\frac{ic}{V_{cb}}\right|_{ie=0}$$



تمرین: پارامترهای هیبرید را محاسبه کنید.

جواب:

$$h_{ib}=\frac{h_{ie}}{h_{ie}h_{oe}+(1+h_{fe})(1-h_{re})}$$

$$h_{fb}=\frac{-h_{fe}(1-h_{re})-h_{oe}h_{ie}}{(1+h_{fe})(1-h_{re})-h_{oe}h_{ie}}$$

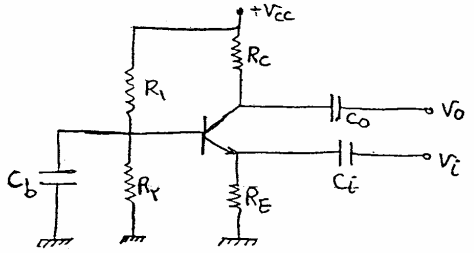
$$h_{ob}=\frac{h_{oe}}{h_{ie}h_{oe}+(1+h_{re})(1+h_{fe})}$$

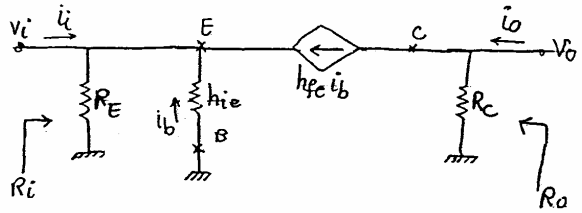
$$h_{rb}=\frac{h_{ie}h_{oe}}{1+h_{fe}}-h_{re}$$

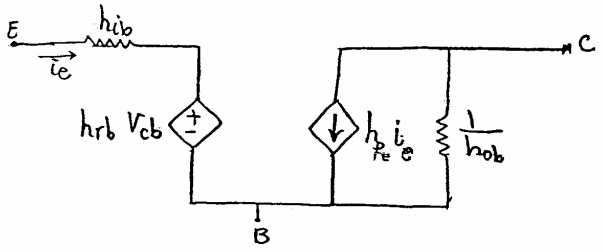
می‌توان از تقریبهای $h_{ie}h_{oe}\ll h_{fe}$

$$\rightarrow h_{ib}=\frac{h_{ie}}{1+h_{fe}} \quad , \quad h_{fb}=\frac{-h_{fe}}{1+h_{fe}} \quad , \quad h_{ob}=\frac{h_{oe}}{1+h_{fe}}$$

تقویت‌کنندهٔ بیس مشترک:

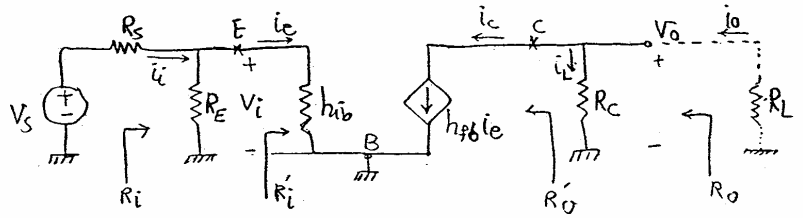






$$h_{ib} = \frac{v_{eb}}{i_e} = \frac{h_{ie}}{1+h_{fe}} \quad , \quad h_{rb} = \frac{v_{eb}}{v_{cb}} = \frac{h_{ie}h_{oe}}{1+h_{fe}} - h_{re}$$

$$h_{fb} = \frac{i_c}{i_e} = \frac{-h_{fe}}{1+h_{fe}} \quad , \quad h_{ob} = \frac{i_c}{v_{cb}} = \frac{h_{oe}}{1+h_{fe}}$$



$$A_i = \frac{i_L}{i_i} = \frac{i_L}{i_c} \cdot \frac{i_c}{i_e} \cdot \frac{i_e}{i_i} = -1 \times h_{fb} \times \frac{R_E}{R_E + h_{ib}}$$

$$\longrightarrow A_i = \frac{-h_{fb}R_E}{R_E + h_{ib}} \simeq -h_{fb}$$

$$R_i = \frac{V_i}{i_i} = R_E \,||\, R'_i$$

$$R'_i = \frac{V_i}{i_e} = \frac{i_e h_{ib}}{i_e} = h_{ib} \longrightarrow R'_i = h_{ib}$$

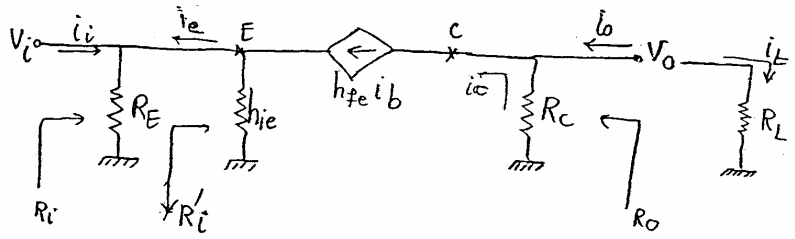
$$\longrightarrow R_i = R_E \,||\, h_{ib} \simeq h_{ib}$$

$$A_V = \frac{V_o}{V_i} = \frac{-R_C i_c}{h_{ib} i_e} = \frac{\overbrace{h_{fb}}^{\text{بعدی منفی}}}{h_{ib}} R_C = -\frac{h_{fe}}{h_{ie}} R_C \longrightarrow A_V = \frac{-h_{fe}}{h_{ie}} R_C$$

$A_V = A_i \dfrac{R_C}{R_i}$: راه دیگر برای بدست آوردن A_V

$$R_o = \left.\frac{V_o}{i_o}\right|_{V_S=0} = R_C \,||\, R'_o = R_C \longrightarrow R_o = R_C$$

$$R'_o = \left.\frac{V_o}{i_c}\right|_{V_S=0} = \infty \longrightarrow R'_o = \infty$$



$$A_i = \frac{i_c}{i_i} = \frac{i_c}{i_e} \cdot \frac{i_e}{i_i} = \frac{h_{fe} i_b}{(1+h_{fe}) i_b} \times \frac{-R_E}{R_E + R'_i} = \frac{-h_{fe}}{1+h_{fe}}$$

$$\longrightarrow \quad A_i = -\frac{h_{fe}}{1+h_{fe}}$$

$$R_i = \frac{V_i}{i_i} = R_E \| R'_i = R_E \| \frac{V_i}{-i_e} = R_E \| \frac{h_{ie}}{1+h_{fe}} \simeq \frac{h_{ie}}{1+h_{fe}}$$

$$\longrightarrow \quad R_i = R_E \| \frac{h_{ie}}{1+h_{fe}} \simeq \frac{h_{ie}}{1+h_{fe}}$$

$$R'_i = \frac{-i_b h_{ie}}{-(1+h_{fe}) i_b} = \frac{h_{ie}}{1+h_{fe}} \quad \longrightarrow \quad R'_i = \frac{h_{ie}}{1+h_{fe}}$$

$$A_V = \frac{V_o}{V_i} = \frac{-R_C i_c}{-i_b h_{ie}} = \frac{h_{fe}}{h_{ie}} R_C \quad \longrightarrow \quad A_V = \frac{h_{fe}}{h_{ie}} R_C$$

$$R_o = \left.\frac{V_o}{i_o}\right|_{V_s=0} = R_C \| R'_o = R_C \| \frac{V_o}{i_i} \simeq R_C \quad \longrightarrow \quad R_o \simeq R_C$$

اگر خازن C_b را از مدار برداریم آن گاه:

$$R_i = \frac{V_i}{i_i} = R_E \| R'_i = R_E \| \frac{V_i}{-i_e} = R_E \| \frac{h_{ie}+R_b}{1+h_{fe}} = \frac{h_{ie}+R_b}{1+h_{fe}}$$

$$R'_i = \frac{-i_b h_{ie} - i_b (R_b)}{-(1+h_{fe}) i_b} = \frac{h_{ie}+R_b}{1+h_{fe}}$$

$$A_V = \frac{V_o}{V_i} = \frac{-R_C i_c}{-i_b h_{ie} - i_b R_b} = \frac{h_{fe} R_C}{h_{ie}+R_b}$$

مثال: تقویت‌کننده بیس مشترک بایپس شده:

$R_E = 1K$, $R_S = 10\Omega$

$h_{ib} = 21.4\Omega$, $R_L = 1K$, $h_{rb} = 2.5 \times 10^{-4}$, $h_{fb} = -0.98$

$h_{ob} = 0.49 \times 10^{-6} S$

$\longrightarrow A_i = -h_{fb} = 0.98$

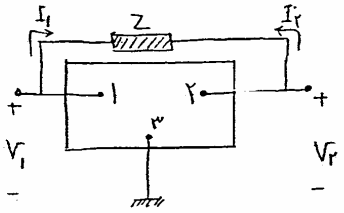
$A_V = \dfrac{-h_{fb} R_L'}{h_{ib}} = 48$, $R_L' = R_L \| R_C$

$R_o = \dfrac{1}{h_{ob}} \| R_C = R_C = 1K\Omega$

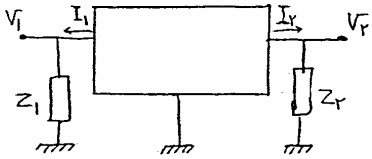
$R_i = h_{ib} \| R_E \simeq h_{ib} = 21.4$, $A_{V_S} = \dfrac{V_o}{V_S} = \dfrac{V_o}{V_i} \cdot \dfrac{V_i}{V_S}$

$A_{V_S} = A_V \cdot \dfrac{R_i}{R_i + R_S} = 31.2$

نوع تقویت‌کننده	A_i	A_V	R_i	R_o	
C.E با خازن بای پاس	h_{fe} بالا	$\frac{-h_{fe}}{h_{ie}} R_C \gg$ بالا	متوسط	بالا	کاربرد فرکانس متوسط
C.E بدون خازن	متوسط	پائین	بالا	بالا	
C.C	متوسط	$\simeq 1$	بالا	پائین	
C.B با خازن بیس	$\simeq 1$	بالا	پائین	بالا	



قضیهٔ میلر:

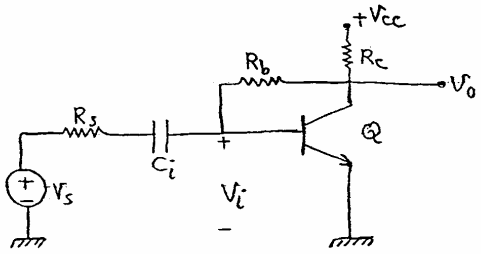


$$\begin{cases} \frac{V_2}{V_1} = K \\ I_1 = -I_2 = \frac{V_1 - V_2}{Z} \end{cases} \longrightarrow Z_1 = \frac{V_1}{I_1} \;,\; Z_2 = \frac{V_2}{I_2} = \frac{KV_1}{V_2}$$

$$\longrightarrow Z_1 = \frac{Z}{1-K}$$

$$Z_2 = \frac{Z}{1-\frac{1}{K}} = \frac{KZ}{K-1}$$

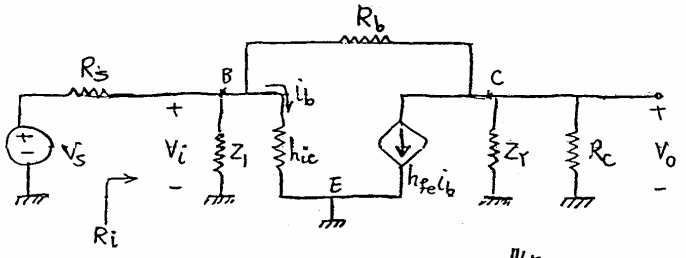
مثال:



$A_V = ?$

$A_{VS} = ?$

$R_i = ?$



$$Z_1 = \frac{Z}{1-K} \quad , \quad Z_2 = \frac{KZ}{K-1} \simeq Z$$

(بازخورد ولتاژ)

$h_{ie} = 1\text{K}\Omega$

$h_{fe} = 100$

$(h_{oe})^{-1} = 40\text{K}$

$R_b = 200\text{K}$

$R_C = 10\text{K}$

$R_S = 10\text{K}$

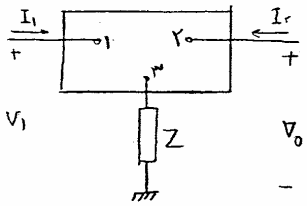
$|A_V| \gg$

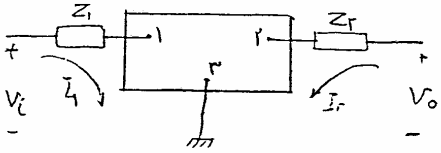
$$A_V = \frac{V_o}{V_i} = \frac{-h_{fe} i_b \left(\frac{1}{h_{oe}} \,\|\, Z_2 \,\|\, R_C\right)}{i_b h_{ie}} \simeq -513$$

$$R_i = Z_1 \,\|\, h_{ie} = 130.19\ \Omega$$

$$A_{VS} = \frac{V_o}{V_S} = \frac{V_o}{V_i} \cdot \frac{V_i}{V_S} = A_V \cdot \frac{R_i}{R_i + R_S} = -12.4\ \Omega$$

قضیهٔ دوم میلر:

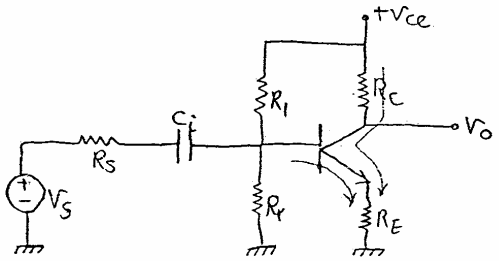


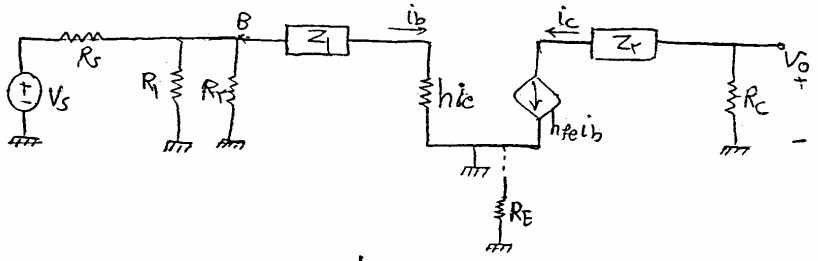


$$\frac{I_2}{I_1}=K \quad , \quad \begin{cases} V_i = V_{13} + Z(I_1+I_2) \\ V_0 = V_{23} + Z(I_1+I_2) \end{cases} \quad , \quad \begin{cases} V_i = Z_1 I_1 + V_{13} \\ V_2 = Z_2 I_2 + V_{23} \end{cases}$$

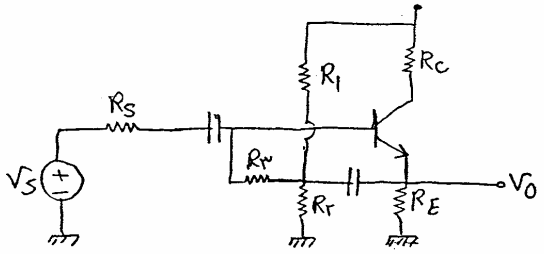
$$\longrightarrow \begin{cases} Z_1 = Z(1+K) \\ Z_2 = \frac{K+1}{K} Z \end{cases}$$

مثال:

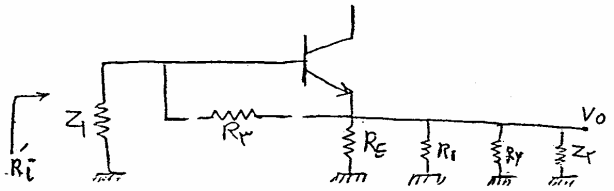




$$Z_1 = R_E(1+h_{fe}) \quad , \quad Z_2 = \frac{1+h_{fe}}{h_{fe}} R_E \simeq R_E \quad , \quad (h_{oe})^{-1} \gg (R_E + R_C)$$



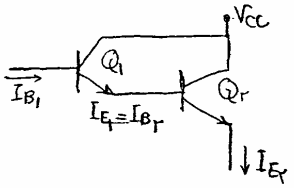
مدار معادل AC:



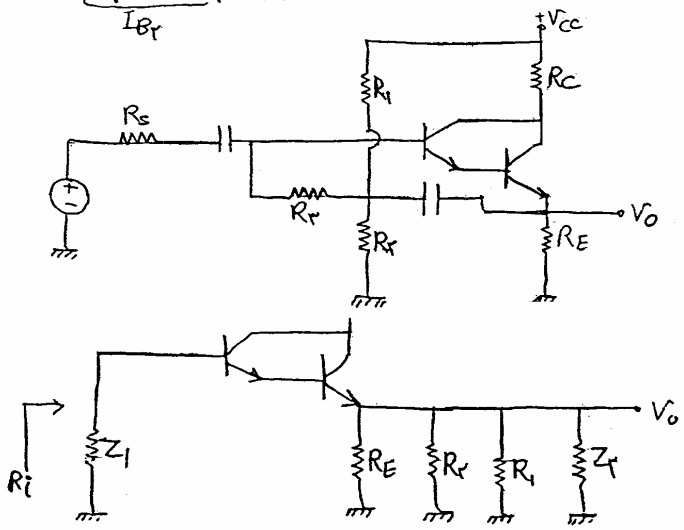
$$R_i' = Z_1 \| \left[h_{fe} + (1+r_e)(R_E \| R_1 \| R_3 \| Z_2) \right]$$

$$Z_1 = \frac{R_2}{1-A_V} \quad , \quad Z_2 = \frac{R_2}{1-\frac{1}{A_V}}$$

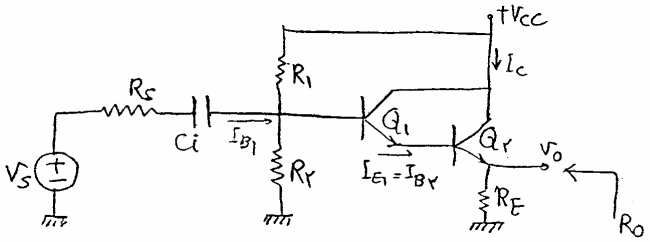
دارلینگتون:



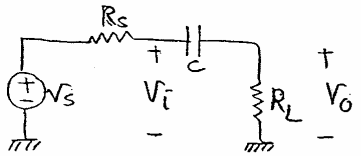
$$I_{E_2} = \frac{I_{B_1}(1+\beta_1)(1+\beta_2)}{I_{B_2}}$$



$$R'_i = Z_1 \| \left[h_{ie_1} + (1+h_{fe_1}) \left[h_{ie_2} + (1+h_{fe_2})(R_E \| R_1 \| R_2 \| Z_2) \right] \right]$$



$$R_O = R_E \| \frac{1}{1+h_{fe_2}} \left[h_{ie_2} + \frac{1}{1+h_{fe_1}} \left[h_{ie_1} + R_1 \| R_2 \| R_S \right] \right]$$



$(R_L+R_S)C = \tau$ ثابت زمانی

$\omega_p = \frac{1}{\tau}$ قطب سیستم

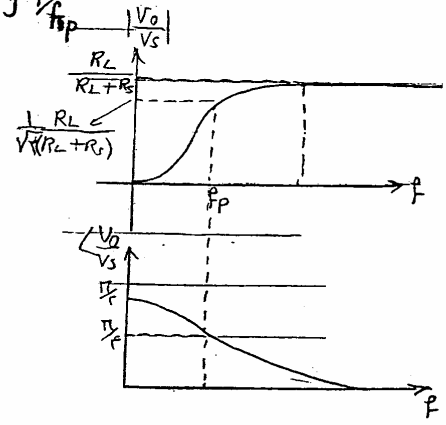
$$\frac{V_o}{V_s} = \frac{R_L}{R_L+R_S+\frac{1}{CS}} = \frac{R_L CS}{(R_L+R_S)CS+1} = \frac{R_L}{R_L+R_S} \cdot \frac{S}{S+p}$$

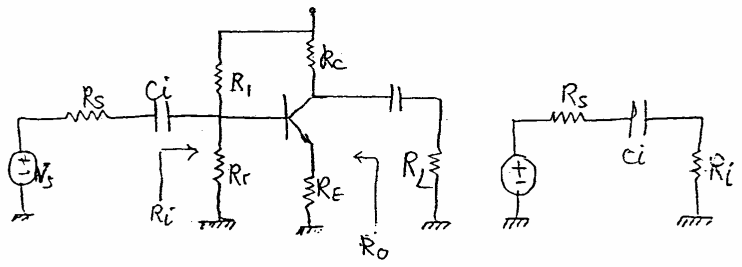
$$\frac{V_o(j\omega)}{V_s(j\omega)} = \frac{jR_L C\omega}{1+j(R_L+R_S)\omega_p C} \qquad \text{if } \omega_p = \frac{1}{(R_S+R_L)}$$

$$\longrightarrow \frac{V_o(j\omega)}{V_s(j\omega)} = \frac{jR_L C\omega}{1+j\frac{\omega}{\omega_p}} = \frac{j2\pi R_L C f}{1+j\frac{f}{f_p}}$$

$$\left|\frac{V_o}{V_s}\right| = \frac{2\pi R_L C f}{\sqrt{1+\left(\frac{f}{f_p}\right)^2}} = \frac{1}{\sqrt{2}}$$

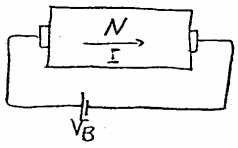
$$\angle\frac{V_o}{V_s} = \frac{\pi}{2} - \text{Arctg}\frac{f}{f_p} = \frac{\pi}{4}$$

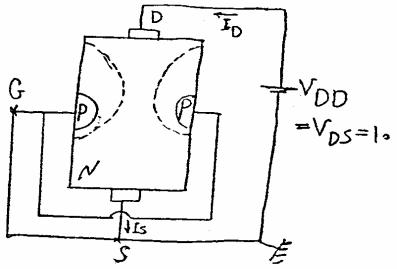


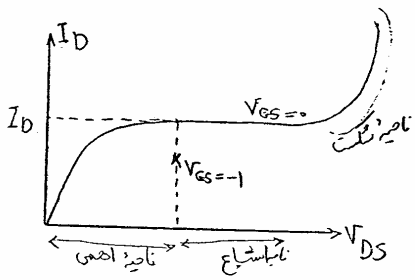


$$f_L = \frac{1}{2\pi(R_i + R_s)C_i}$$

FET : (ترانزیستور اثر میدانی)(field effect transistor)

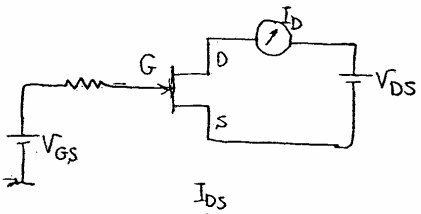


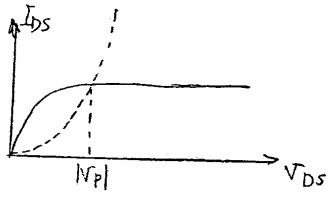




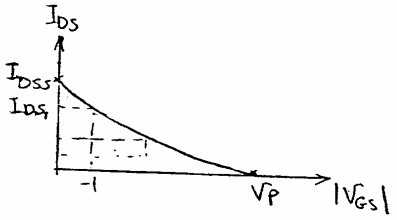
$I_{DSS} \longrightarrow V_{GS}=0$

$V_{GS}=V_P \longrightarrow I_D=0$
قطع





مشخصهٔ انتقال:



$V_{GS}=0 \longrightarrow I_{DS}=I_{DSS}$

$V_{GS}=V_P \longrightarrow I_{DS}=0$

$$I_{DS}=I_{DSS}\left(1-\left|\frac{V_{GS}}{V_P}\right|\right)^2$$

مثال عددی:

$V_P=-4V$
$I_{DSS}=12mA$ $\longrightarrow$
$V_{GS}=0$
$V_{GS}=-1.2$
$V_{GS}=-2V$

$V_{GS}=0 \longrightarrow I_{DS}=I_{DSS}=12mA$

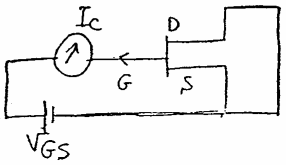
$V_{GS}=-1.2V \longrightarrow I_{DS}=12\left(1-\frac{-1.2}{-4}\right)^2=5.88\ mA$

$V_{GS}=4 \longrightarrow I_{DS}=3\ mA$

$I_G=10nA$

$P_D=0.5\ W$,

$T=-45^\circ t+30^\circ$



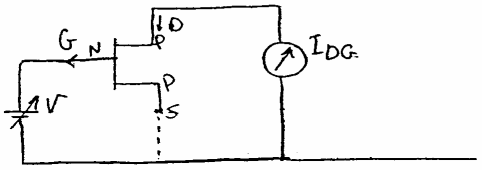
$I_{GSS}=0.01\ \mu A$

$V_{GS}=10V$

$T=100^\circ \longrightarrow I_{GSS}=1\ \mu A$

$V_{GS}=10V$

در حالتی که خطچین نیست



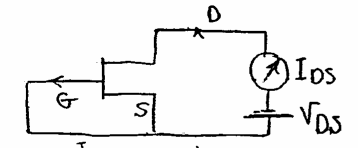
$BV_{DG_0}=-20V$

۲۰ ۲۴ ۲۸

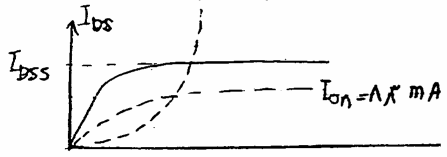
$10\mu A$

در حالتی که خطچین وجود دارد:

$BV_{DG_0}=-BV_{GSS}$



$V_{GS}=0 \longrightarrow I_{DSS}=I_{DS}$

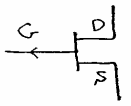


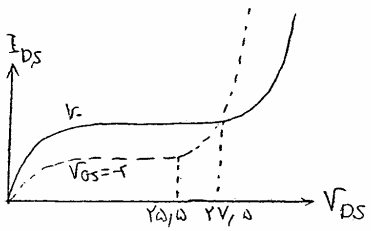
$V_{DS}=10V$

$V_{GS}=3.5V$

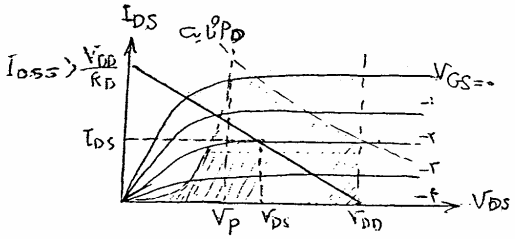
$I_{D_{off}} = 10\,nA$
$V_{DS} = 12\,V$ $\longrightarrow V_{GS} = 8\,V \simeq V_P$

BV_{DS}



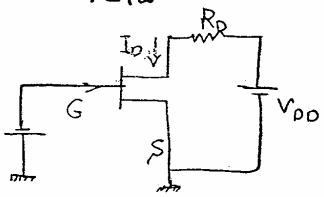


$BV_{DS_0} = -27.5$, $V_{DS} = V_{DG} + V_{GS}$



$P_D = I_{DS} V_{DS}$

$T = 25°$

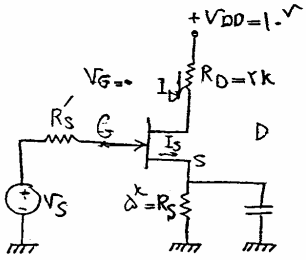


معادله‌ی خط بار $V_{DD} = R_D I_D + V_{DS}$

ناحیه‌ی اشباع $V_{GS} = 0$ ، $V_{DS} = |V_P|$

$\boxed{V_{DS} \geq V_{GS} - V_P}$

مثال : V_{GS} ، I_{DS} ، V_P را برای مدار نشان داده شده بدست آورید



$I_{DSS} = 5\,mA$, $V_P = -5\,V$

$$\begin{cases} V_{GS} = V_G - V_S = -V_S = -R_S I_{DS} \\ I_{DS} = I_{DSS}\left(1 - \frac{V_{GS}}{V_P}\right)^2 = I_{DSS}\left(1 + \frac{R_S I_{DS}}{V_P}\right)^2 \end{cases}$$

$\longrightarrow$ I_{DS} 

$\longrightarrow$ $I_{DS} = \frac{-V_{GS}}{R_S} = 1.04$

$$\longrightarrow \quad -\frac{V_{GS}}{R_S} = I_{DSS}\left(1-\frac{V_{GS}}{V_P}\right)^2 \quad \longrightarrow \quad V_{GS} = \begin{cases} -3{,}2 \\ -1{,}8 \end{cases}$$

$$\begin{cases} I_{DS} < I_{DSS} \\ |V_{GS}| < |V_P| \end{cases}$$

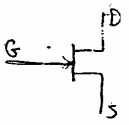
شرایطی که باید حتماً در مدار رعایت چک شود.

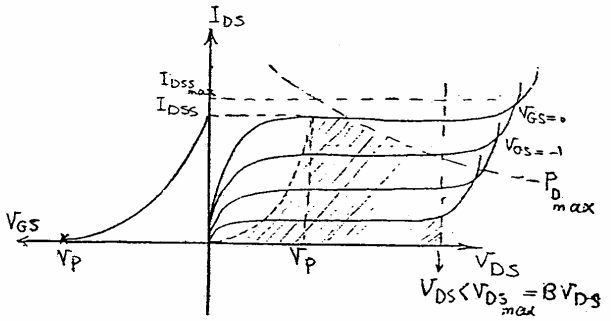
$$V_{DS} = V_D - V_S = V_{DD} - R_D I_{DS} = R_S \cdot I_{DS}$$

$$\longrightarrow V_{DS} = 5{,}4\ V$$

$$V_{DS} \geq V_{GS} - V_P \quad \longrightarrow \quad V_{DS} \geq -3{,}2 - (-5) = 1{,}8\ V$$

چک کردن برای ناحیهٔ مجاز



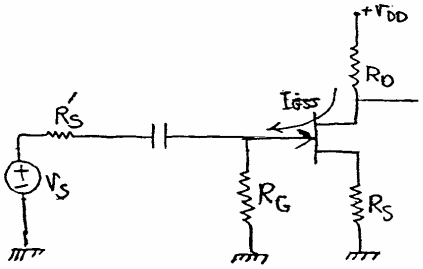


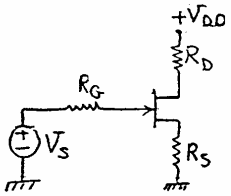
$$\begin{cases} V_{DS} \gg V_{GS} - V_P \\ BV_{DS} \\ I_{DS_{max}} \\ P_{D_{max}} = V_{DS} \cdot I_{DS} \end{cases}$$

پارامترهای محدودکننده

$$I_{DS} = I_{DSS}\left(1 - \left|\frac{V_{GS}}{V_P}\right|\right)^2$$

$$I_{DS} < I_{DSS}$$





① I_{GSS}

② $V_G = I_{GSS} \times R_G = 10^{nA} \times 100^{M} = 1\ V$

③ $I_{GSS} = 10\ nA$

④ $V_{GS} = V_G - V_S = V_G - R_S I_S$

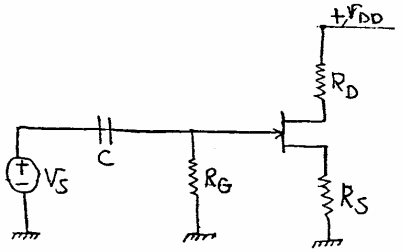
$= 1 - 4 = -3$

⑤ $I_{DS} - I_{GSS} = I_S$

R_G اگر کوچک باشد دیگر امپدانس ورودی آن خیلی بزرگ نخواهد بود و اگر خیلی بزرگ باشد با تغییرات دما که I_{GSS} تغییر می‌کند V_G تغییر خواهد کرد و احتمال این است که FET از ناحیه اشباع خارج شود. همچنین با توجه به اینکه در ورودی سیگنال‌های noise وجود دارند اگر R_G خیلی بزرگ باشد این سیگنال به خروجی منتقل می‌شود و در خروجی با توان بالایی تقویت و ظاهر می‌شود امّا اگر R_G مناسب باشد noise توسط R_G به زمین منتقل می‌شود و در خروجی ظاهر نخواهد شد.

①, ②, ③ $\longrightarrow$ $V_{GS} = R_S I_{DS} + (R_S + R_G) I_{GSS}$

مثال:



$25^\circ < T < 100^\circ$

$I_{GSS}(25^\circ) = 10\ nA$

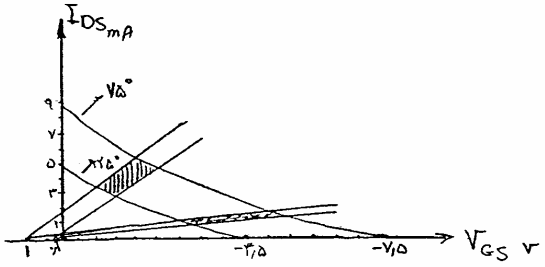
$\Delta T = 5^\circ C \longrightarrow I_{GSS} \times 10$

$I_{DS} = I_{DSS}\left(1 - \left|\frac{V_{GS}}{V_P}\right|\right)^2$

25° { $I_{DSS} = 5\ mA$, $V_P = -4.5\ V$ } 100° { $I_{DSS} = 9\ mA$, $V_P = -1.5\ V$ }

a) $R_S = 500\ \Omega$ b) $R_S = 5\ K\Omega$

مشخصه انتقالی را رسم کنید.



a) $R_S = 500\ \Omega$

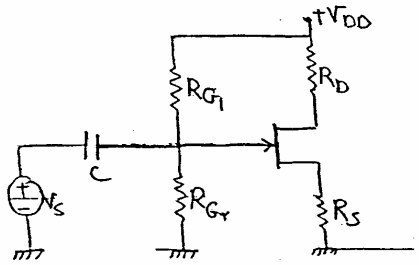
$$25^\circ \longrightarrow V_{GS} = -500 I_{DS} + 0.1$$

$$V_{GS} \simeq -500 I_{DS} + 1$$

b) $R_S = 5\ k\Omega$

$$20^\circ \longrightarrow V_{GS} = -5000 I_{DS} + 0.1$$

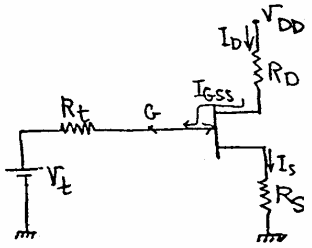
$$V_{GS} = -5000 I_D + 1$$



$$V_{GS} = V_G - V_S$$

$$V_{GS} = V_{DD} \times \frac{R_{G_2}}{R_{G_1} + R_{G_2}} - R_S I_S$$

$$\begin{cases} V_t = \dfrac{R_{G_2}}{R_{G_1} + R_{G_2}} V_{DD} \\ R_t = R_{G_1} \parallel R_{G_2} \end{cases}$$

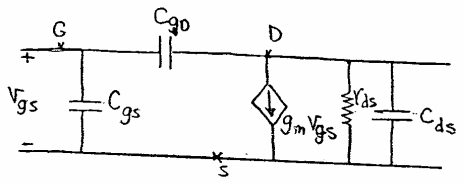


$$\begin{cases} I_D = I_S + I_{GSS} \\ V_G = R_t \times I_{GSS} + V_t \\ V_S = -R_S I_S \end{cases} \quad , \quad V_{GS} = V_G - V_S$$

تحلیل ac و تقویت کننده ها :

C.S	G ورودی	D خروجی	$\|A_V\| > 1$
C.D	G ورودی	S خروجی	$A_V \simeq 1$
C.G	S ورودی	D خروجی	$A_V > 1$ ← کاربرد چندانی ندارد

مدار معادل :



$C_{gs}, C_{gd} \simeq PF$

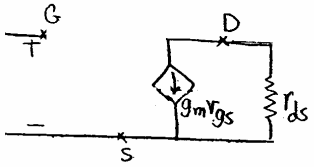
$C_{ds} \ll C_{gs}, C_{gd}$

مقادیری که در کاتالوگ FET داده می‌شوند.

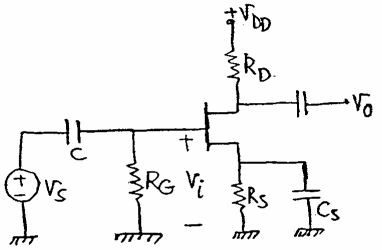
$C_{iss} = C_{gs} + C_{gd}$ ← خازن ورودی (وقتی خروجی اتصال کوتاه است)

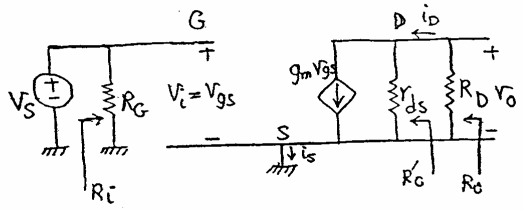
$C_{rss} \simeq C_{gd}$ ← خازن خروجی (وقتی ورودی اتصال کوتاه است)

مدل سیگنال کوچک FET :



تقویت کننده سورس مشترک C.S :

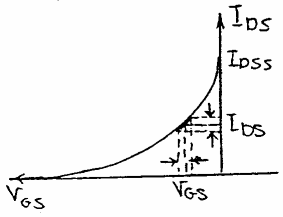




$$A_V = \frac{V_o}{V_i} = \frac{-g_m V_{gs}\,(R_D \| R_{ds})}{V_{gs}} = -g_m\,(R_D \| R_{ds})$$

$$\begin{cases} g_m = \dfrac{\Delta I_{DS}}{\Delta V_{GS}} = g_{m_0}\left(1 - \dfrac{V_{GS}}{V_P}\right) \\ g_{m_0} = \dfrac{2 I_{DSS}}{|V_P|} \end{cases}$$

g_{m_0} شیب مخصص در نقطه I_{DSS}



$$R_i = R_G$$

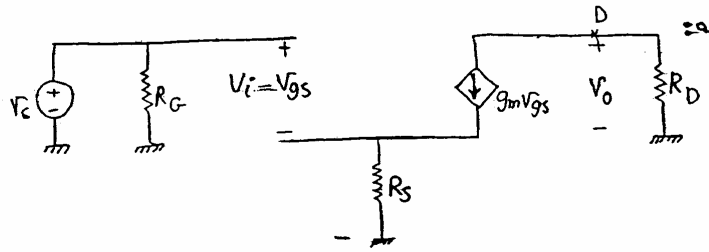
$$R_o = \left.\frac{V_o}{i_o}\right|_{V_s=0} \quad , \quad R_o = R_D \| R'_o$$

$$R'_o = \frac{V_o}{i_D} = r_{ds} \longrightarrow R_o = R_D \| r_{ds}$$

باتوجه به اینکه V_s از نظر ac زمین است درنتیجه $V_i = V_{GS}$ لذا در این نوع تقویت کننده ها علاوه بر پارامترهای بالا باید V_{ipp} را نیز محاسبه و محدود کنیم.

$$V_{ipp} = \frac{V_{opp}}{A_V}$$

درحالت بایپاس نشده:

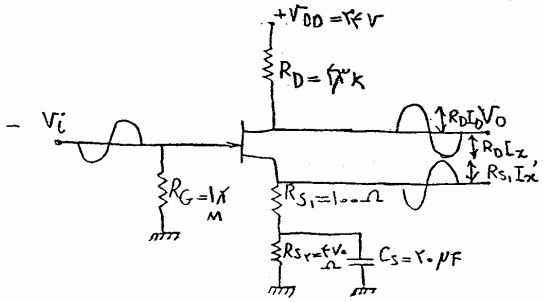


$$A_V = \frac{V_o}{V_i} = \frac{-g_m V_{gs} R_D}{V_{gs} + V_{gs} g_m R_S} = \frac{-g_m R_D}{1 + g_m R_S}$$

$$\longrightarrow A_V = \frac{-g_m R_D}{1 + g_m R_S}$$

$$R_i = R_G \quad , \quad R_o = R_D$$

مثال :



$I_{DSS} = 4\ mA$

$V_P = -4\ V$

$R_i , R_o , A_V , V_{opp} , \beta_L = ?$

$$\begin{cases} I_{DS} = I_{DSS}\left(1 - \left|\frac{V_{GS}}{V_P}\right|\right)^2 \\ V_{GS} = V_G - V_S = 0 - I_{DS}(R_{S1} + R_{S2}) = -1.5 I_{DS} \end{cases} \longrightarrow \begin{cases} I_{DS} = 2.98\ mA \\ V_{GS} = -1.47\ V \end{cases}$$

$$g_m = \frac{2 I_{DSS}}{|V_P|}\left(1 - \frac{V_{GS}}{V_P}\right) = 1.413\ mS \qquad (g_{m_0} = 2\ mS)$$

$$A_V = \frac{-g_m R_D}{1 + g_m R_{S1}} = -0.12 \quad , \quad R_i = R_G = 1.2\ M\Omega$$

$$R_o = R_D = 6.3\ M\Omega \quad , \quad V_D = V_{DD} - R_D I_D$$

$$V_{op}^{+} = R_D I_D \longrightarrow V_{op}^{+} = 11.8\ V$$

(dc) $V_S = R_{S1} I_{DS} + R_{S2} I_{DS}$

(ac) $V_s = R_{S1} I_D$

$$V_{op}^{-} = V_{DS} \times \frac{R_D}{R_{S1} + R_D}$$

نقطه Q

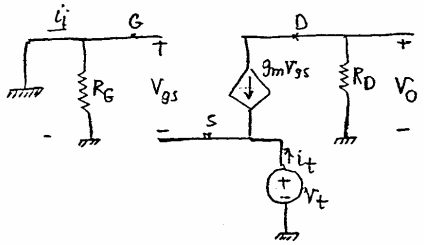
(dc) $V_{DS} = V_D - V_S = V_{DD} - R_D I_D - I_D(R_{S1} + R_{S2}) = 9.05\ V$

$$\longrightarrow V_{op}^{-} = 9.34\ V$$

$$\longrightarrow \boxed{V_{opp} = 2 \times 9.34 = 18.68\ V}$$

مقاومت سورس کانکس

$$R_{CS} = R_{S_2} \| (R_{S_1} + r_s)$$



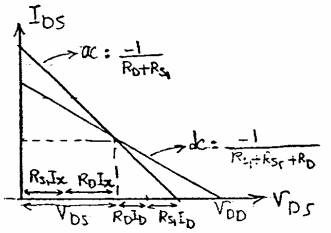
$$i_t = -g_m V_{gs}$$

$$V_t = -V_{gs} \longrightarrow r_s = \frac{V_t}{I_t} = \frac{1}{g_m}$$

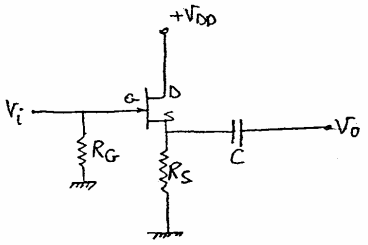
$$\longrightarrow R_{CS} = 4V_o \| (100 + V_{18}) \simeq 300\,\Omega$$

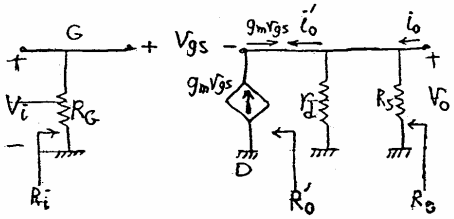
$$\longrightarrow f_L = \frac{1}{2\pi R_{CS} \cdot C_{es}} = 2915\ Hz$$

روش دیگر یافتن V_{opp} از روی خط بار ac، dc ←



تقویت کننده دربین مشترک C.D :





$$A_V = \frac{V_o}{V_i} = \frac{g_m V_{gs} (r_d \| R_S \| R'_L)}{V_{gs} + g_m V_{gs} (r_d \| R_S)}$$

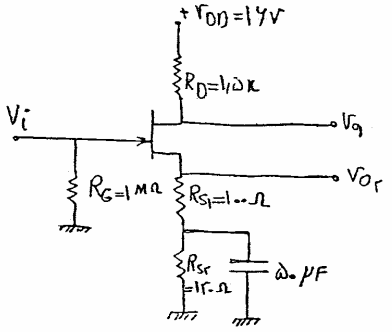
$$\longrightarrow A_V = \frac{g_m R'_L}{1 + g_m R'_L} < 1 \quad , \quad R_i = R_G$$

$$R_o = \frac{V_o}{i_o}\Big|_{V_i = 0} = R'_o \| (r_d \| R_S)$$

$$\longrightarrow R_o = \frac{R'_o}{g_m} \| (r_d \| R_S) \simeq \frac{1}{g_m} \| R_S$$

$$R'_o = \frac{V_o}{i'_o} = \frac{-V_{gs}}{-g_m V_{gs}} = \frac{1}{g_m}$$

مثال:



$I_{DSS}=12\ mA$

$g_{m_0}=4.5\ ms$

$R_{o1}, R_{o2}, A_{v1}, A_{v2}, R_i, f_L = ?$

$$I_{DS}=I_{DSS}\left(1-\frac{V_{GS}}{V_P}\right)^2$$

$$V_{GS}=V_G-V_S=0-(R_{S1}+R_{S2})I_{DS}$$

$$g_{m_0}=\frac{2I_{DSS}}{|V_P|}=4.5\ ms$$

$\Rightarrow V_P=-5.33\ V$

$\Rightarrow \begin{cases} I_{DS}=4.5\ mA \\ V_{GS}=-1.14\ V \end{cases}$

$$g_m=g_{m_0}\left(1-\frac{V_{GS}}{V_P}\right)=3.33\ ms$$

(C.S) : $$A_{V1}=\frac{-g_m R_D}{1+g_m R_{S1}}=-3.74$$

(C.D) : $$A_{V2}=\frac{V_{o2}}{V_i}=\frac{g_m R_L'}{1+g_m R_L'}=\frac{g_m R_{S1}}{1+g_m R_{S1}}=0.78$$

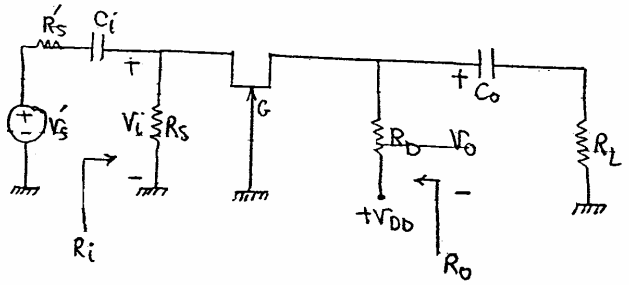
$R_i=R_G=1\ M\Omega$ ، $R_{o1}=R_D=1.5K$

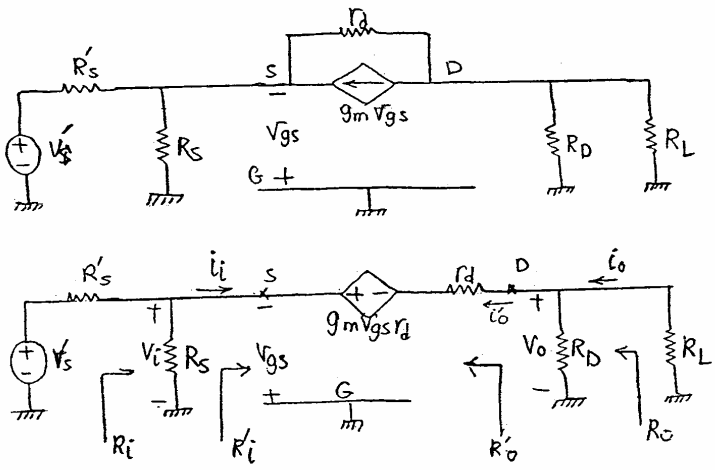
$R_{o2}=\frac{1}{g_m}\|R_{S1}=75\ \Omega$ ، $r_s=\frac{1}{g_m}=301$

$f_L=?$ $\rightarrow$ $R_{CS}=R_{S2}\|\left[R_{S1}+\frac{1}{g_m}\right]=64.15\ \Omega$

$\rightarrow$ $f_L=\frac{1}{2\pi R_{CS}C_S}=48.9\ Hz$

تقویت‌کنندهٔ گیت‌مشترک C.G :





$$A_V = \frac{V_o}{V_i} =$$

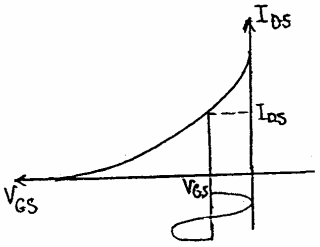
$$V_o = (R_D \| R_L) i_i \qquad KVL: \; +V_{gs} + g_m V_{gs} r_d i_i + r_d i_i + (R_D \| R_L) i_i = 0$$

$$V_i \overset{*}{=} -V_{gs}$$

$$\longrightarrow \; i_i \overset{*}{=} -V_{gs} \frac{1 + g_m r_d}{r_d + (R_D \| R_L)}$$

$$\longrightarrow A_V = \frac{V_o}{V_i} = \frac{(R_D \| R_L)\left[\frac{V_{gs}(1+g_m r_d)}{r_d + (R_D \| R_L)}\right]}{-V_{gs}}$$

$$\longrightarrow A_V = \frac{(R_D \| R_L)(1 + g_m r_d)}{r_d + (R_D \| R_L)}$$



$$V_D = V_{DD} - R_D I_D$$

$$V_i \downarrow \qquad I_{DS} \uparrow \qquad V_D \downarrow$$

$$A_V \simeq \frac{(R_D \| R_L)(g_m r_d)}{r_d} \simeq g_m (R_D \| R_L) \longrightarrow A_V \simeq g_m (R_D \| R_L)$$

$$R_i = \frac{V_i}{i'_s} = R_S \| R'_i \qquad , \qquad R'_i = \frac{V_i}{i_i} \overset{*}{=} \frac{-V_{gs}}{-V_{gs}\frac{1+g_m r_d}{r_d + (R_D \| R_L)}} \simeq \frac{1}{g_m}$$

$$\longrightarrow \; R'_i = \frac{r_d + (R_D \| R_L)}{1 + g_m r_d} \simeq \frac{1}{g_m}$$

$$\longrightarrow R_i = R_S \,||\, \left(\frac{r_d + (R_D||R_L)}{1+g_m r_d}\right) \simeq R_S \,||\, \frac{1}{g_m}$$

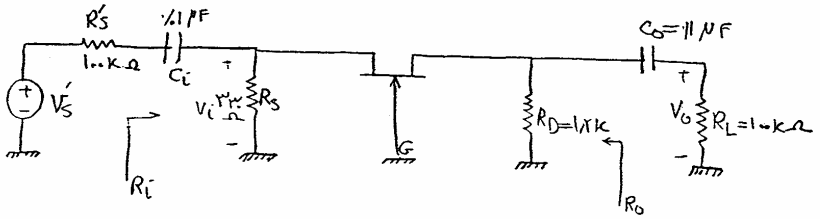
$$R_o = \left.\frac{V_o}{i_o}\right|_{V_S=0} = R_D || R'_o$$

$$R'_o = \frac{V_o}{i'_o} = \frac{r_d i'_o + g_m (V_{gs}) r_d + i'_o (R_S||R'_S)}{i'_o} = r_d + g_m r_d (R_S||R'_S) + (R_S||R'_S)$$

($-(R_S||R'_S) i'_o$)

$\because r_d \longrightarrow R'_o = r_d \left(1 + g_m (R_S||R'_S)\right)$

$$\longrightarrow R_o = R_D \,||\, \left[r_d \left(1 + g_m (R_S||R'_S)\right)\right] \simeq R_D$$



مثال :

$V_{GS} = -1.11\,V$, $g_m = 1.1\,mS$, $r_d = \infty$

R_i , R_o , A_V , f_L = ?

$$A_V = \frac{(1+g_m r_d)}{r_d + R'_L} \times R'_L \simeq R'_L \left(\frac{1}{r_d} + g_m\right) \longrightarrow A_V = g_m R'_L = g_m (R_L || R_D) = 1.1\Omega$$

$$R_i = R_S \,||\, \frac{1}{g_m} = 11.1\,\Omega \quad , \quad R_o = R_D = 1.1\,K$$

$$R_{Ci} = R_i + R'_S \simeq 100\,k\Omega \quad , \quad \tau_{Ci} = R_{Ci} \times C_i = 1\,ms$$

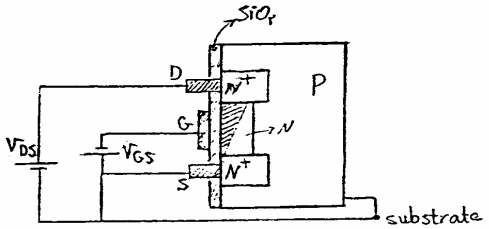
$$R_{Co} = R_D + R_L \simeq 100\,k\Omega \quad , \quad \tau_{Co} = R_{Co} \times C_o = 1.\,ms$$

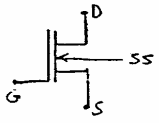
$$, \quad f_{Ci} = \frac{1}{2\pi\tau_{Ci}} = 159\,Hz$$

MOS FET : دونوع از این تقویت کننده داریم .

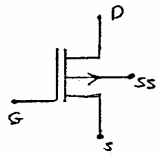
۱- تخلیه‌ای Depletion ۲- افزایشی Enhancement

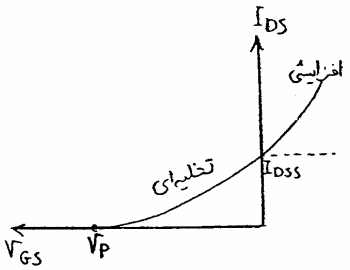
نوع تخلیه‌ای :

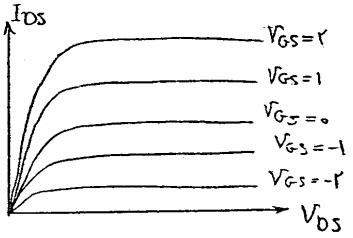




کانال N







$$I_{DS} = I_{DSS}\left(1 - \frac{V_{GS}}{V_P}\right)^2 \quad , \quad g_m = g_{m_0}\left(1 - \frac{V_{GS}}{V_P}\right)$$

$$g_{m_0} = \frac{2 I_{DSS}}{|V_P|}$$

مثال :

$I_{DSS} = 18\ mA$, $V_P = -5\ V$

الف- N کانال

$V_{GS} = -3 \longrightarrow I_{DS} = 18\left(1 - \frac{-3}{-5}\right)^2 = 2{,}88\ mA$

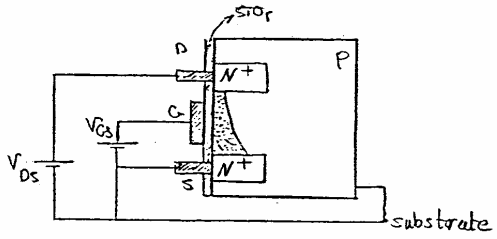
$V_{GS} = 2{,}5 \longrightarrow I_{DS} = 18\left(1 - \frac{2{,}5}{-5}\right)^2 = 40{,}5\ mA$

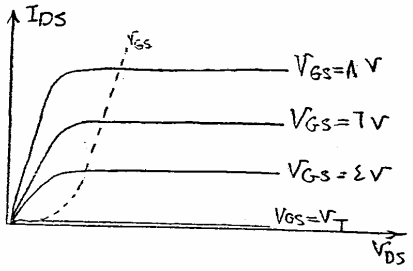
ب- P کانال $I_{DSS} = 18\ mA$, $V_P = 5\ V$

$V_{GS} = -3 \longrightarrow I_{DS} = 49{,}08\ mA$

$V_{GS} = 2{,}5^V \longrightarrow I_{DS} = 18\ mA$

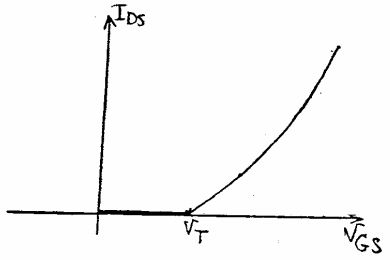
۲-نوع افزایشی :

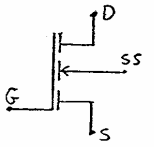




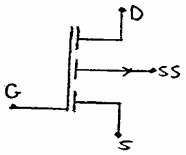
$V_T = V_{GD} \simeq ۱.۳$ ولت

ولتاژ آستانه‌ی تشکیل کانال





کانال N

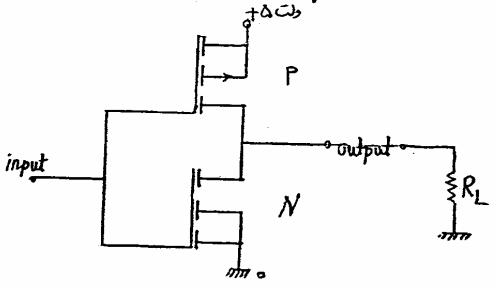


کانال P

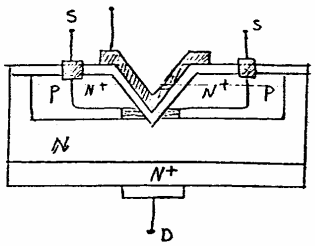
$$I_D = \frac{1}{2}\beta (V_{GS} - V_T)^2 \quad , \quad V_{GS} \geqslant V_T \quad , \quad \beta \simeq ۱۰ \times ۱۰^{-۳} \ A/V^2$$

$$V_{DS_{sat}} = V_{GS} - V_T$$

از ترکیب NMOS (یا NMOSFET) و PMOS المانی به نام CMOS بوجود می‌آید.

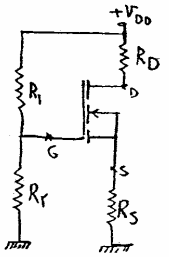


VMOS :



کاربرد VMOS در مدارهای سوئیچینگ با جریان بالا است چون مقاومت کمی دارد.

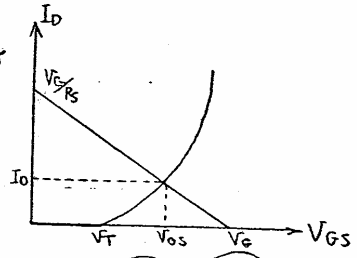
مدارهای بایاس MOSFET :



$I_D = \frac{1}{2}\beta (V_{GS} - V_T)^2$

$V_G = \frac{R_2}{R_1+R_2} V_{DD}$

$V_S = R_S I_D$



$\longrightarrow V_{GS} = V_G - V_S = V_G - R_S I_D \longrightarrow \boxed{I_D = \frac{V_G}{R_S} - \frac{V_{GS}}{R_S}}$

$I_D = \frac{-B - \sqrt{B^2 - 4AC}}{2A}$ در حالات کلی NMOS , PMOS

$A = R_S^2$, $B = -2\left[(|V_G| - |V_T|)R_S + \frac{1}{\beta}\right]$, $C = (|V_G| - |V_T|)^2$

مثال : $V_{DD} = 12$, $R_D = 2.2\,k$, $R_2 = 22\,M\Omega$, $R_1 = 47\,M\Omega$, $R_S = 500\,\Omega$, $\beta = 0.5 \times 10^{-3}\ A/V^2$, $V_T = 2\,V$

$\longrightarrow I_D = \frac{1}{2} \times 0.5 \times 10^{-3}(V_G - 2)^2$, $I_D = \frac{V_G}{R_S} - \frac{V_{GS}}{R_S}$

$V_G = \frac{22}{22+47} \times 12 = 3.84\,V \longrightarrow \boxed{I_D = \frac{3.84}{500} - \frac{V_{GS}}{500}}$

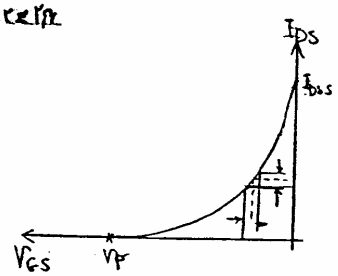
$V_{DS} = V_D - V_S = (V_{DD} - R_D I_D) - R_S I_D = 11.4\,V$

$|V_{DS}| > |V_{GS} - V_T|$ — $11.4 > 1.84$ — قابل قبول

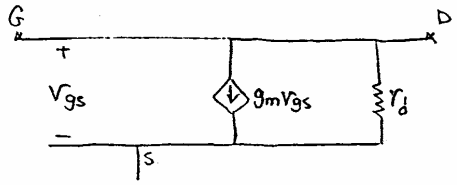
$g_m^{-1} = \frac{\Delta V_{GS}}{\Delta I_{DS}} \longrightarrow g_m = \frac{\Delta I_{DS}}{\Delta V_{GS}}$

JFET , Depletion :

$$\begin{cases} I_{DS} = I_{DSS}\left(1 - \frac{V_{GS}}{V_P}\right)^2 \\ g_m = \frac{2 I_{DSS}}{|V_P|}\left(1 - \frac{V_{GS}}{V_P}\right) \end{cases}$$

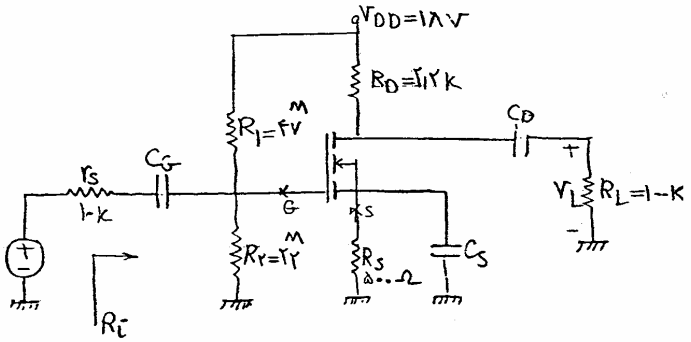


MOSFET Enhancement : $\begin{cases} \frac{dI_D}{\Delta V_{GS}} = \text{٪۵۰ } \beta(V_{GS}-V_T) = g_m \\ \beta(V_G - V_T) = g_m \end{cases}$



در حالت کلی برای اینکه در ناحیه فعال قرار داشته باشیم : $|V_{DS}| \geq |V_{GS}-V_T|$

مثال :



۱- ناحیهٔ فعال ؟

۲- R_i

۳- $A_{VS}=\frac{V_L}{V_S}$

$V_T=۲V$. $\beta=٪۵\times۱۰^{-۳}\ A/V^2$, $r_d=۷۵K$, $I_D=۱,۹\ mA$

$\longrightarrow V_{DS} \geq V_{GS}-V_T \longrightarrow ۱۲,۸V \geq ۴,۷۹-۲$

$V_{DS} = V_D - V_S = (V_{DD} - R_D I_D) - (R_S I_D) = ۱۲,۸۷\ V$

$V_{GS} = V_G - V_S = ۴,۷۹\ V$

$V_G = V_{DD} \times \frac{R_2}{R_1+R_2} = ۵,۷۴\ V$

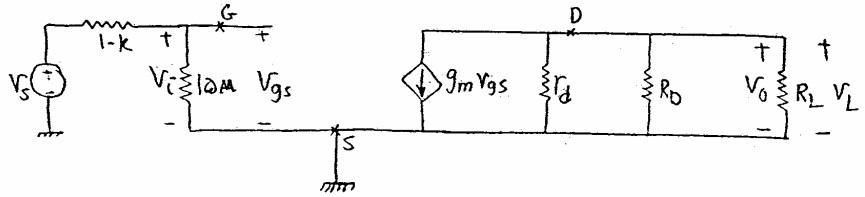
$I_D = \frac{-B-\sqrt{B^2-4AC}}{A}$, $A = +R_S^2$

$B = -2\left[(|V_G|-|V_T|)R_S + \frac{1}{\beta}\right]$

$C = (|V_G|-|V_T|)^2$

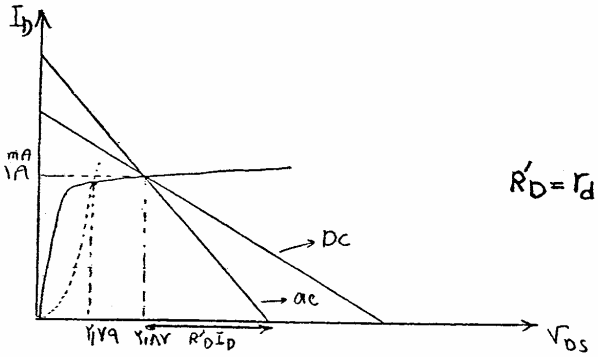
۲۵۱

$$R_{in} = R_1 \| R_2 = 47 \| 22 = 15\ M\Omega$$



$$g_m = \beta (V_{GS} - V_T) = 1.4\ mS$$

$$A_{VS} = \frac{V_L}{V_S} = \frac{V_L}{V_i} \cdot \frac{V_i}{V_S} = \frac{-g_m V_{gs} (R_D \| R_L \| r_d)}{V_{gs}} \times \frac{10 \times 10^6}{10 \times 10^6 + 10 \times 10^3} = -2.94$$

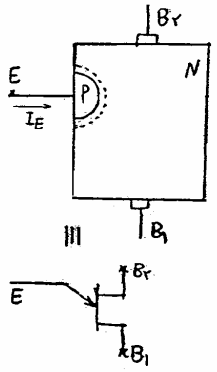


تعیین سوئینگ :

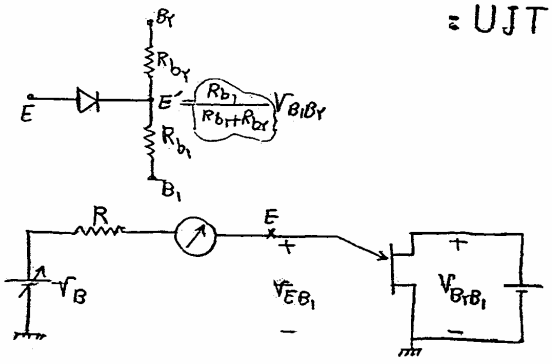
$$R'_D = r_d \| R_D \| R_L$$

خط بار dc : $V_{DD} = V_{DS} + (R'_D + R_S) I_D$

خط بار ac : $V_{DS} = -R'_D I_D$



: UJT

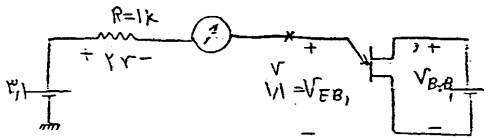


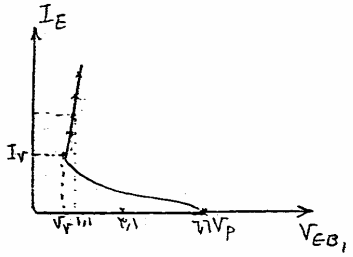
$$\eta = \frac{R_{b_1}}{R_{b_1} + R_{b_2}}$$

بعد از روشن شدن دیود ⟶ ↗ تا حد ⟶ $R_{b_1}\downarrow$ ⟶ $V_{EB_1}\downarrow$

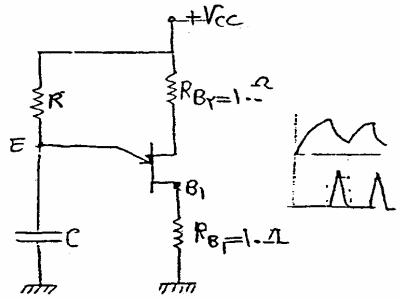
$V_P = V_D + V_E'$

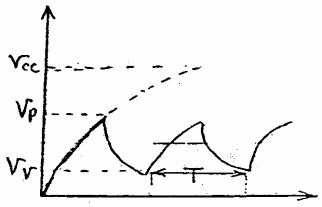
$V_P = V_D + \eta V_{B_2B_1}$





استفاده از UJT در نوسان سازی:





$T \simeq \frac{1}{RC} Ln \frac{1}{1-\eta}$

$V_P = \eta V_{CC} + V_D$

اگر به جای R از منبع جریان استفاده کنیم خازن به صورت خطی شارژ می‌شود:

$CV_P = Q = I \times T \longrightarrow T = \frac{CV_P}{I}$

کاربرد دیگری از UJT: